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*1st June 2023*

## ASX ANNOUNCEMENT

# BURRACOPPIN PROJECT

## *96Mt MAIDEN INFERRED (JORC 2012) COMBINED MINERAL RESOURCE ESTIMATE*

### HIGHLIGHTS

- **Maiden Inferred (JORC 2012) Mineral Resource Estimate for the Company's multi-commodity Rare Earth Elements (REE) + kaolin/halloysite project, comprising;**
  - **36Mt at 1,356ppm Total Rare Earth Oxides (TREO) of Rare Earth bearing material (using 400ppm TREO cut-off) within the -45µm size fraction, contained within the global resource**
    - **This equates to 20,000t of combined TREO products**
  - **An estimated global inferred resource of 96Mt @ ISO-B 80 (using an ISO-Brightness (ISO-B) cut-off of 70) of kaolinite/halloysite bearing material, comprising**
    - **51Mt @ ISO-B 83 of ultra bright white kaolinite/halloysite (>80 ISO-B) bearing material and;**
    - **29Mt @ ISO-B 78 of bright white kaolinite/halloysite (>75<80 ISO-B) bearing material and,**
    - **16Mt @ ISO-B 73 of white kaolinite/halloysite (>70<75 ISO-B) bearing material**
      - **This equates to 36.9Mt of kaolin product & 2.1Mt of halloysite product**
- **Resource is within less than 5% of Ragusa's 100% owned tenure with significant resource expansion upside potential**
- **The Burracoppin Project has multi-commodity development potential with REE product + kaolin/halloysite (compared to stand-alone REE projects)**

Ragusa Minerals Limited (ASX: RAS) ("Ragusa" or "Company") is pleased to advise that it has completed its maiden mineral resource estimate (JORC 2012) at the Company's 100% owned multi-commodity REE and kaolinite/halloysite Burracoppin Project in Western Australia.

A maiden 96Mt at 80 ISO-B inferred kaolinite/halloysite resource has been defined at the project using an ISO-B cutoff of 70, which includes 36Mt at 1,356ppm TREO (using a 400ppm cut-off). Refer Table 1 for REO resource details and Table 2 for global kaolinite/halloysite resource details.

Ragusa Chair, Jerko Zuvela said "***The Company is very excited to have completed its maiden JORC 2012 inferred Mineral Resource Estimate at our 100% owned Burracoppin Project – a true multi-commodity development opportunity for highly valued and strategic critical minerals, including TREO/Rare Earth Elements (REE) and kaolin/halloysite.***

***The shallow and high-grade REE mineralisation alongside the kaolinite and halloysite is very exciting and adds significant potential to the project.***"

**Table 1**. Burracoppin Inferred Mineral Resource Estimate of Rare Earth Oxides using a cut-off of 400ppm TREO

| Rare Earth Oxide Resource | | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| **VOLUME** | **TOTAL** | **DENSITY** | **-45µm** | **-45µm** | **TREO** | **TREO** | **La2O3** | **CeO2** | **Pr6O11** | **Nd2O3** | **Sm2O3** | **Dy2O3** | **Tb4O7** | **Y2O3** |
| **(m³)** | **(t)** | **(g/cm³)** | **%** | **(t)** | **(ppm)** | **(t)** | **(ppm)** | **(ppm)** | **(ppm)** | **(ppm)** | **(ppm)** | **(ppm)** | **(ppm)** | **(ppm)** |
| 23,339,000 | 35,709,000 | 1.53 | 41.3 | 14,731,000 | 1356.4 | 20,000 | 320.4 | 634.1 | 62.5 | 204.2 | 28.1 | 11.7 | 2.6 | 54.6 |

**Table 2**. Burracoppin Inferred Mineral Resource Estimate of Halloysite and Kaolinite bearing material using an ISO-B cut-off of 70

| Global Resource | | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| **ISO-B** | **VOLUME** | **Total** | **DENSITY** | **ISO Brightness** | **-45µm** | **-45µm** | **Halloysite** | **Halloysite** | **Kaolinite** | **Kaolinite** | **Al2O3** | **Fe2O3** | **SiO2** | **TiO2** |
| **%** | **(m3)** | **(t)** | **(g/cm³)** | **%** | **%** | **(t)** | **%** | **(t)** | **%** | **(t)** | **%** | **%** | **%** | **%** |
| **White 70 - 75** | 10,516,000 | 16,080,000 | 1.53 | 73 | 41.2 | 6,630,000 | 3.6 | 238,000 | 73.2 | 4,852,000 | 31.8 | 1.2 | 52.3 | 1.1 |
| **Bright 75 - 80** | 19,002,000 | 29,073,000 | 1.53 | 78 | 47.2 | 13,720,000 | 3.9 | 528,000 | 79.3 | 10,886,000 | 34.0 | 0.9 | 50.8 | 0.6 |
| **Ultra Bright >80** | 33,233,000 | 50,847,000 | 1.53 | 83 | 49.2 | 25,013,000 | 5.3 | 1,321,000 | 84.4 | 21,116,000 | 35.5 | 0.6 | 49.6 | 0.5 |
| **TOTAL** | 62,751,000 | 96,008,000 | | 80 | 47.2 | 45,363,000 | 4.6 | 2,087,000 | 81.2 | 36,854,000 | 34.5 | 0.8 | 50.3 | 0.6 |

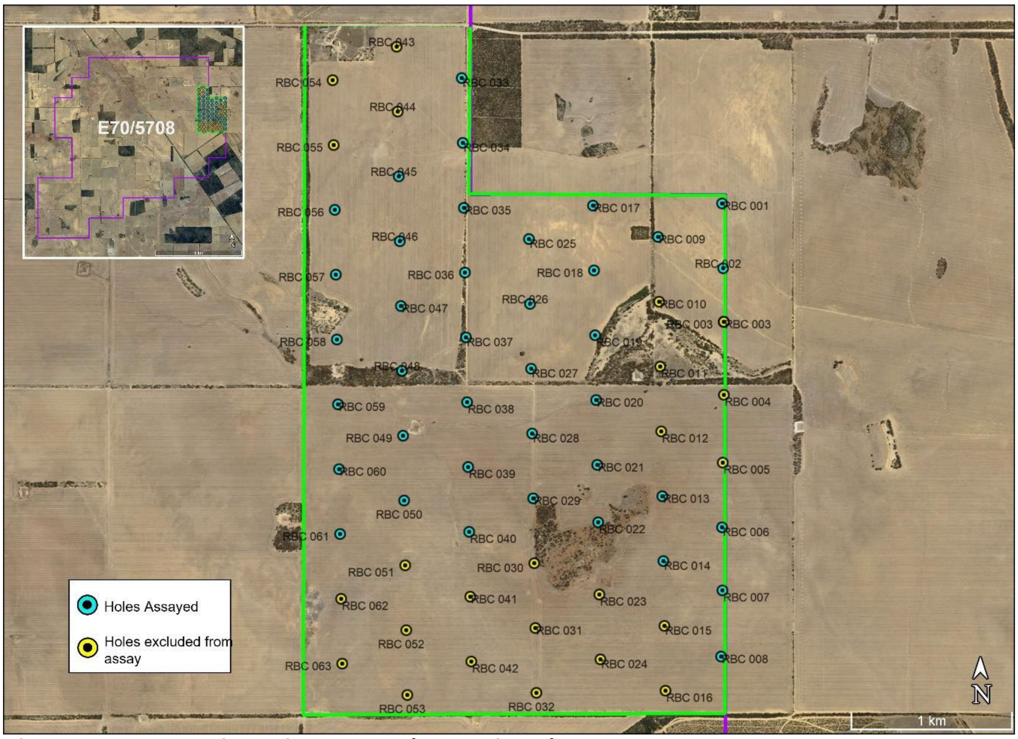


*Figure 1. Burracoppin Project – Sample Location Plan*

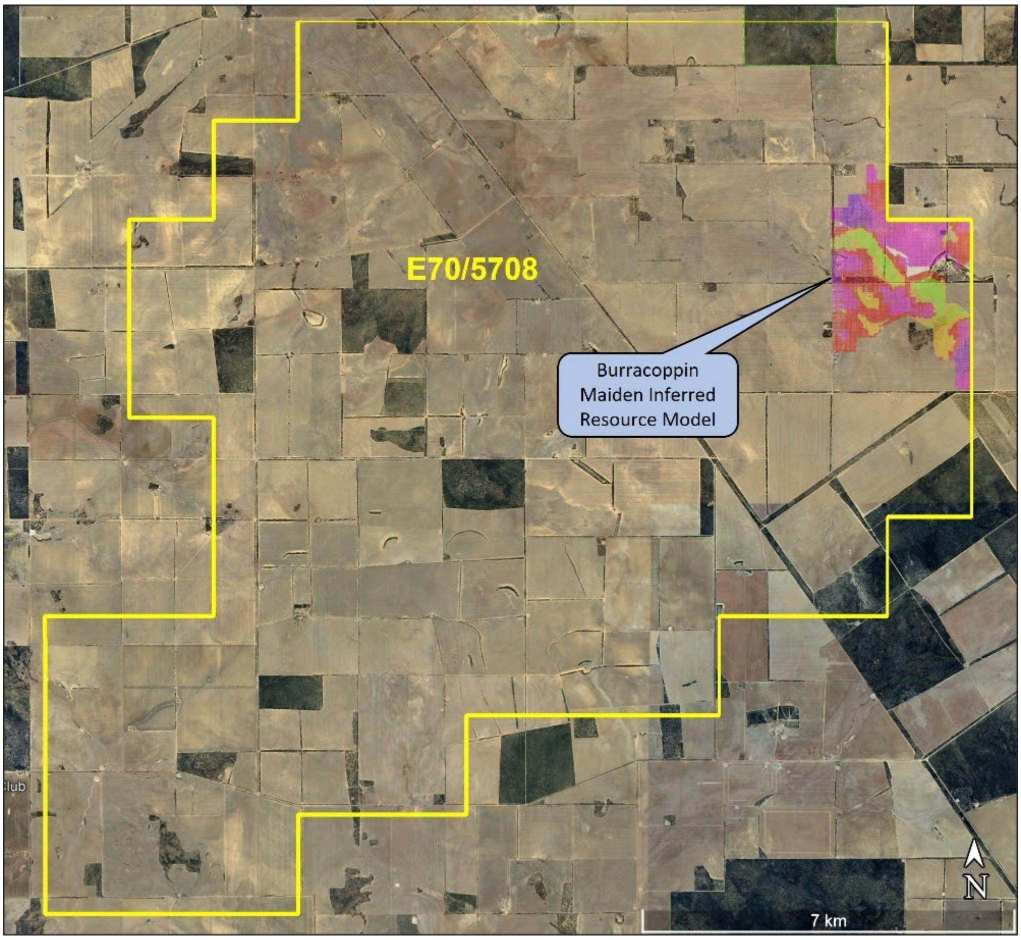


*Figure 2. Burracoppin Project – Resource as a subset of tenure*

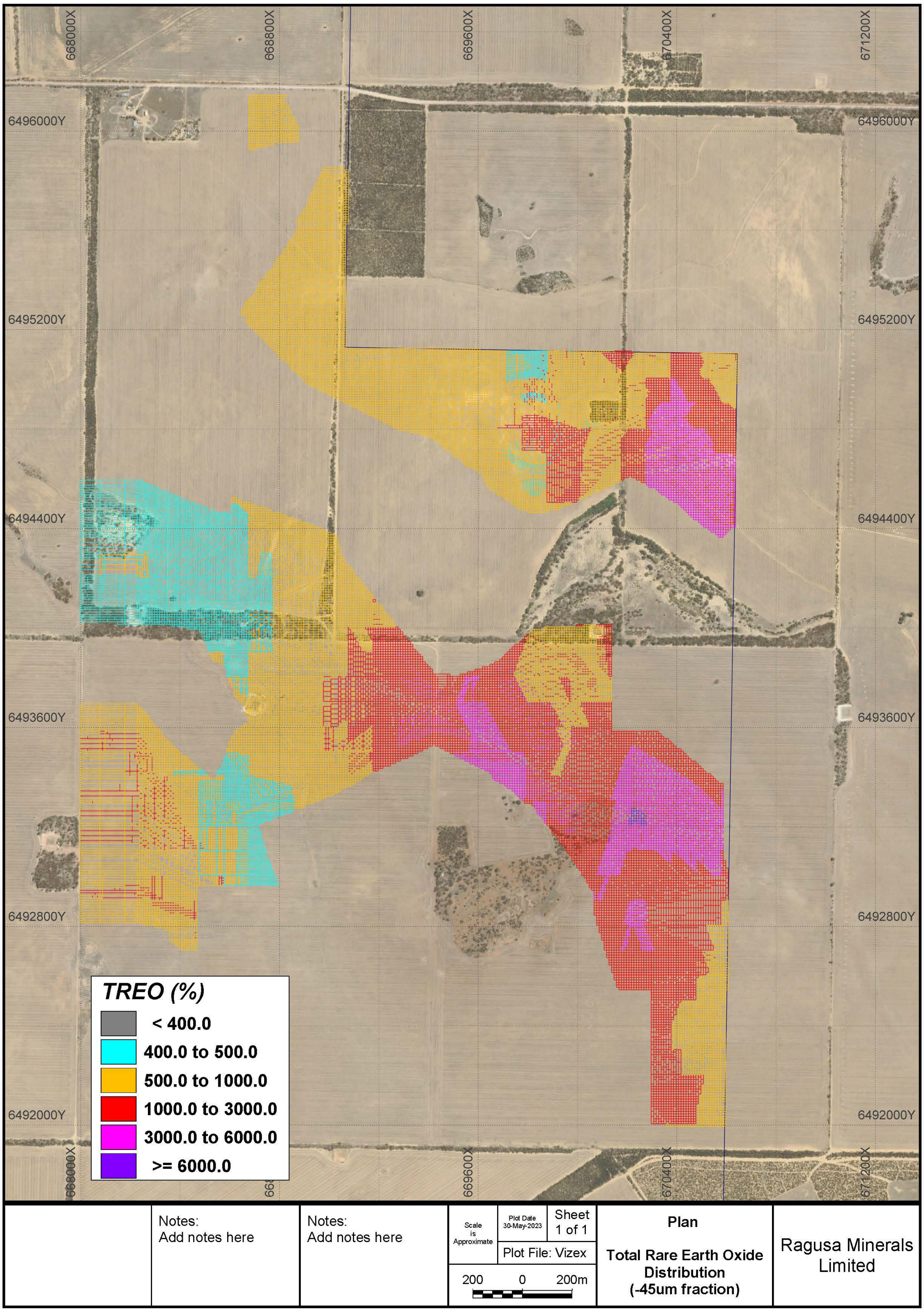


***Figure 3. Burracoppin Project – Indicative TREO distribution in plan view***

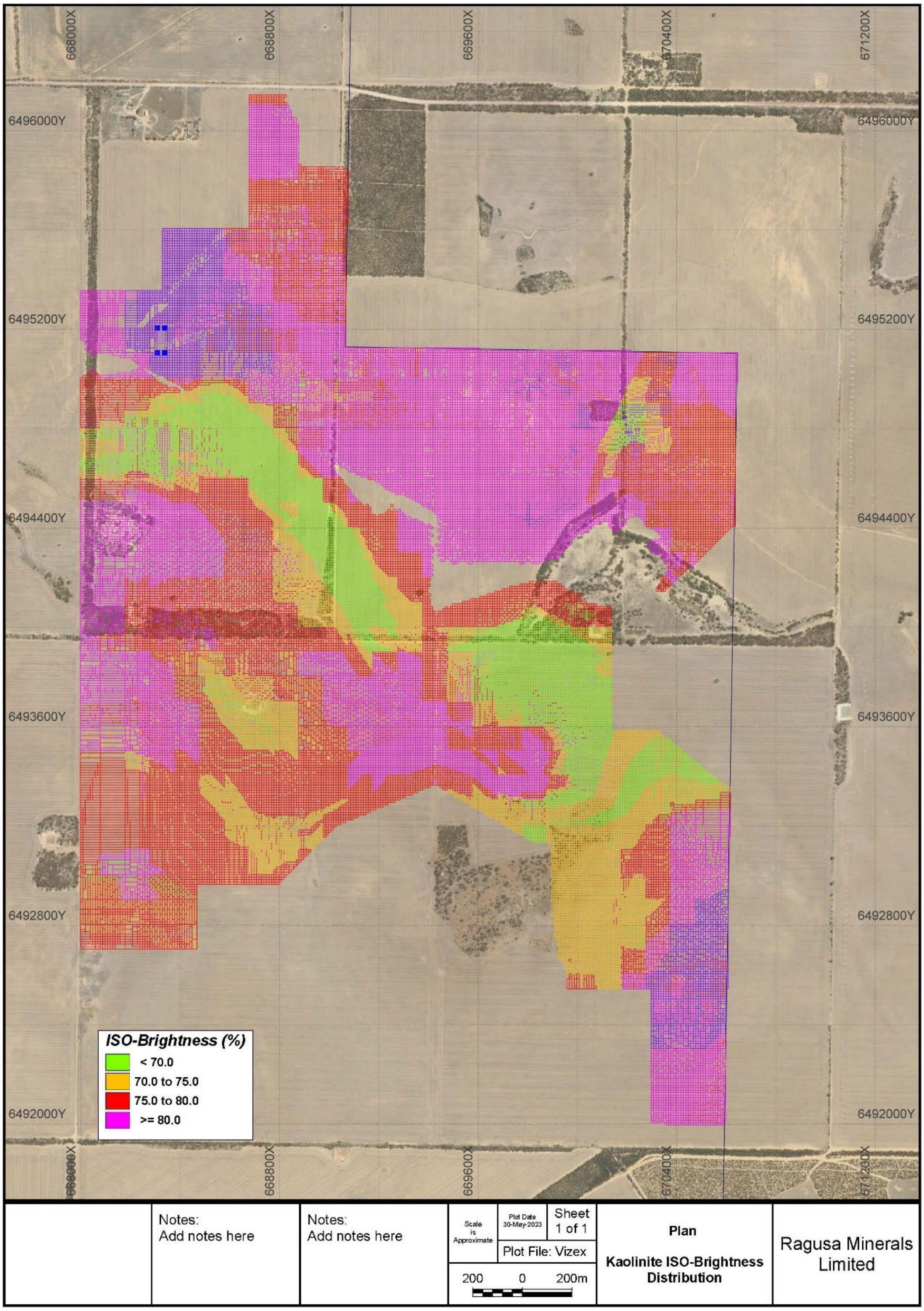


*Figure 4. Burracoppin Project – Indicative ISO-Brightness distribution in plan view*

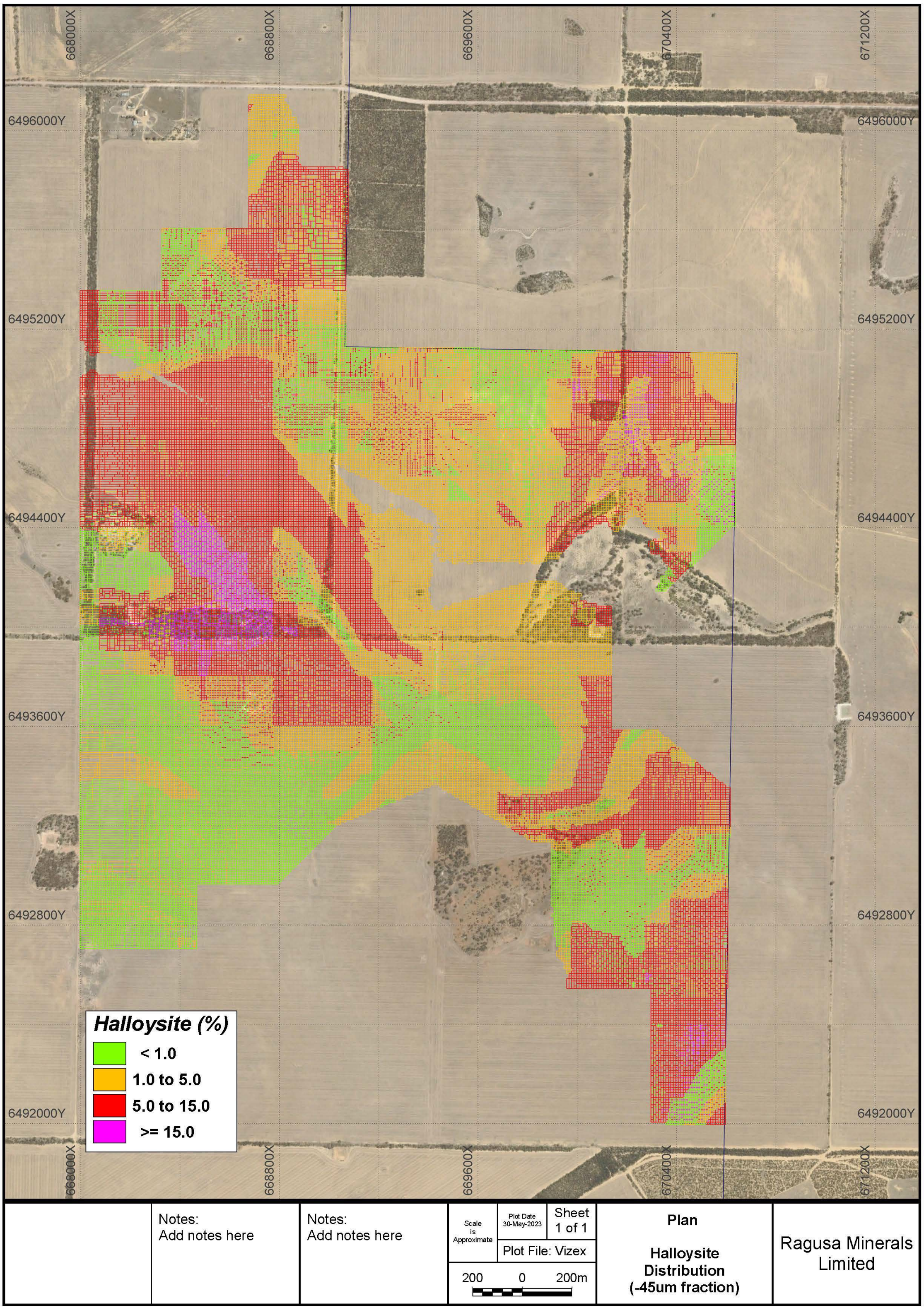


*Figure 5. Burracoppin Project – Indicative Halloysite distribution in plan view*

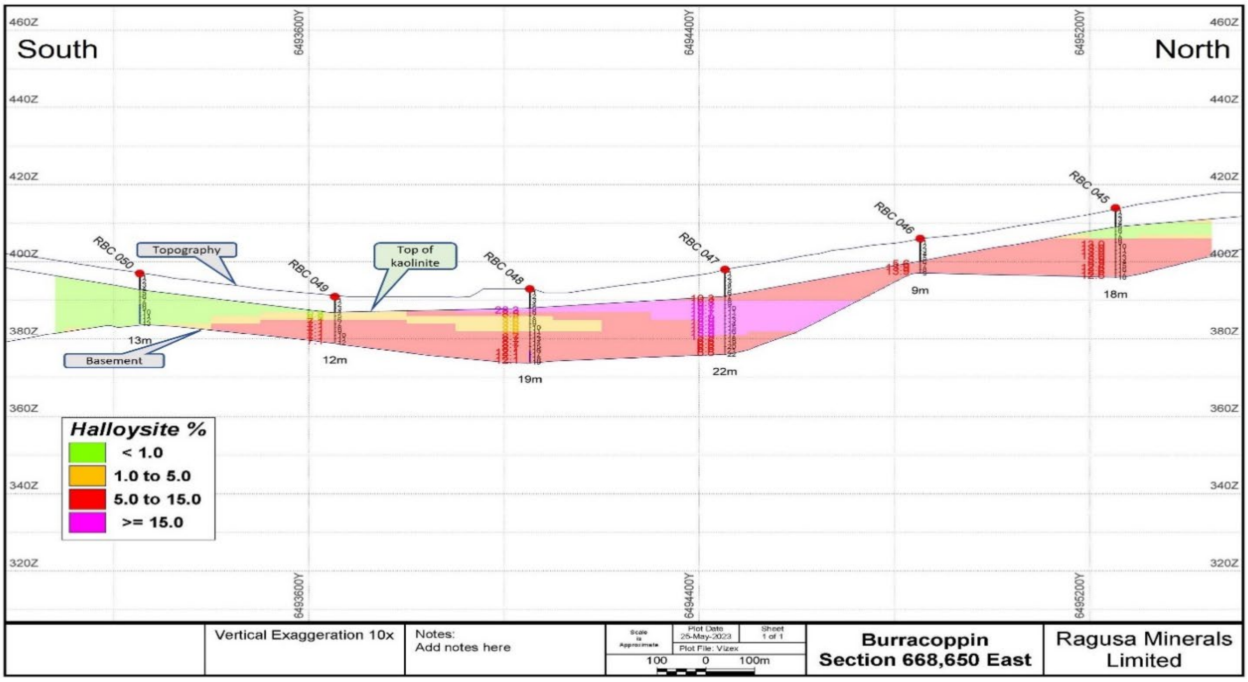


*Figure 6. Burracoppin Project – Section 668, 650 East Halloysite content*

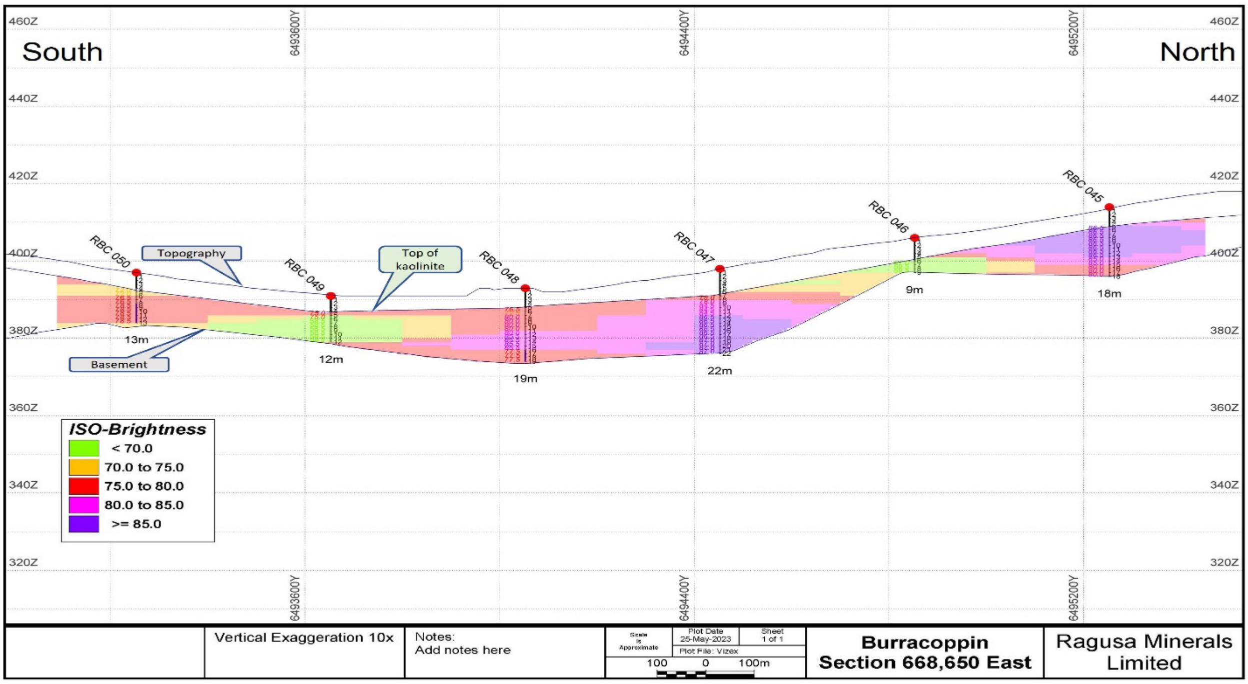


*Figure 7. Burracoppin Project – Section 668, 650 East ISO-Brightness*

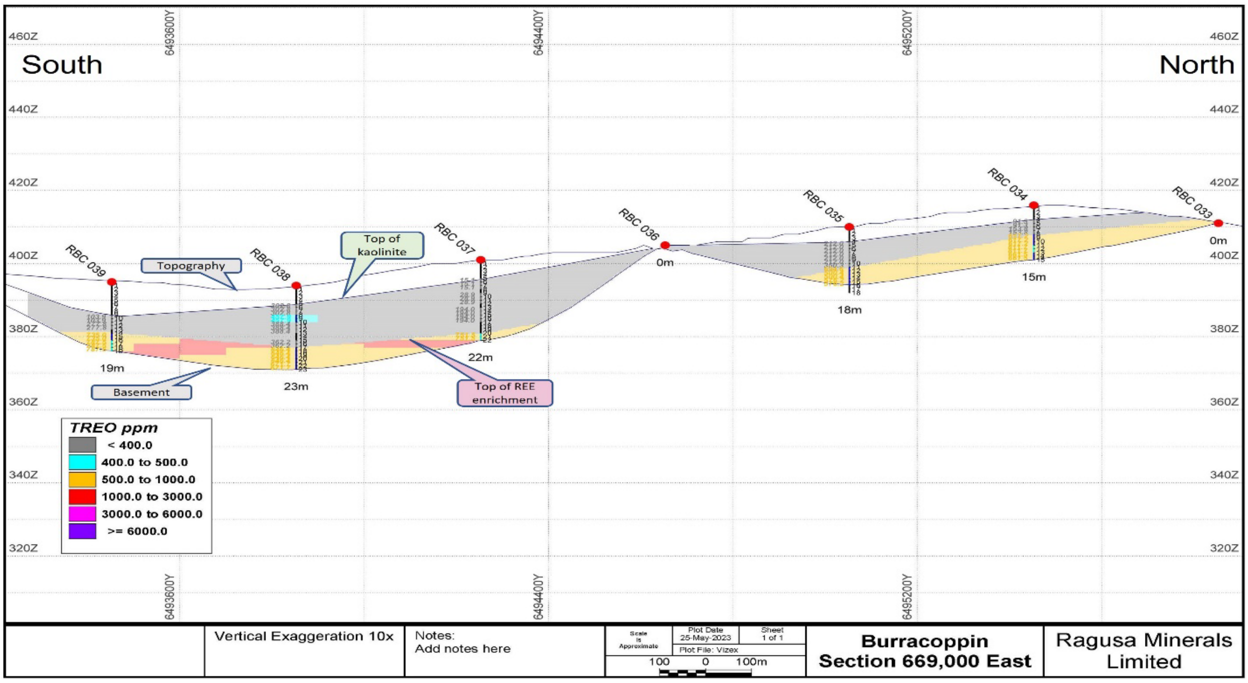


*Figure 8. Burracoppin Project – Section 669,000 East Total Rare Earth Oxide content*

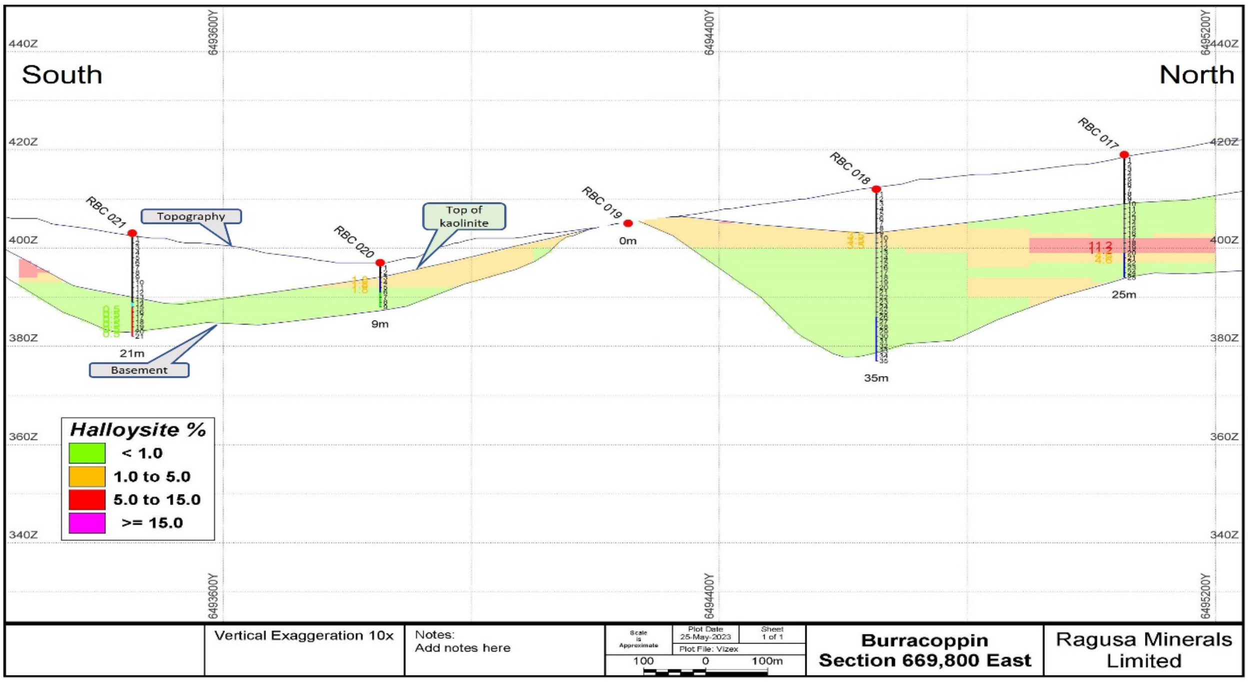


*Figure 9. Burracoppin Project – Section 669, 800 East Halloysite content*

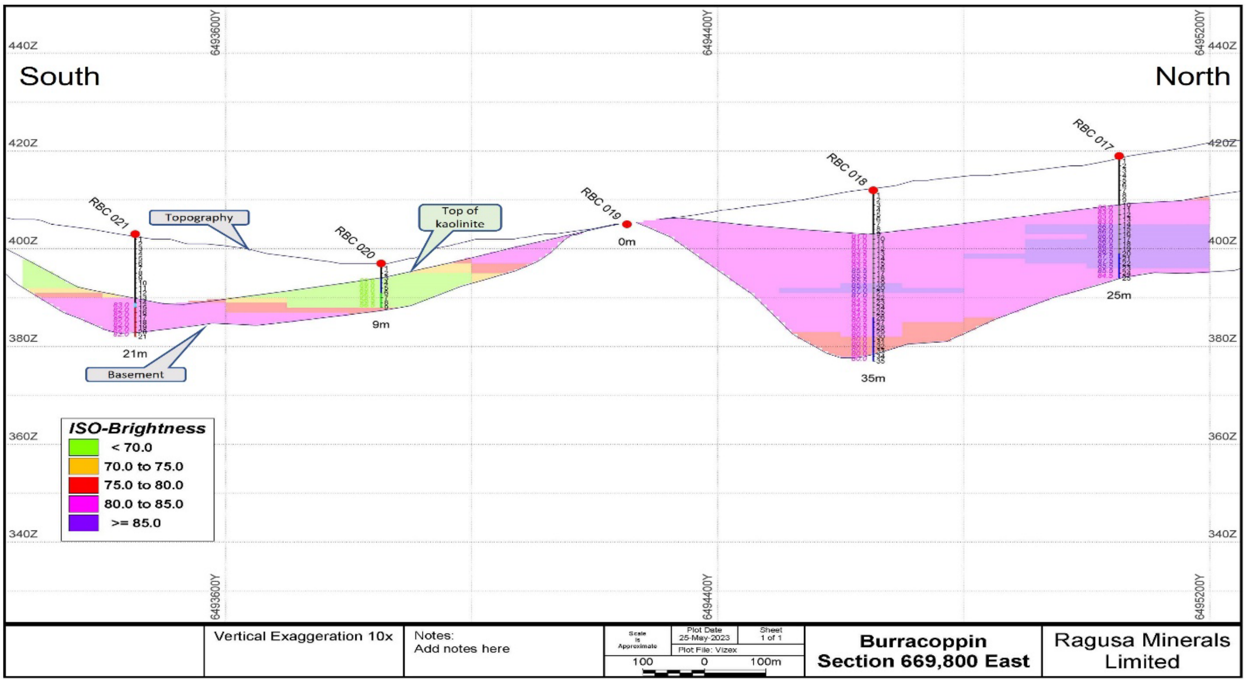


*Figure 10. Burracoppin Project – Section 669, 800 East ISO-Brightness content*

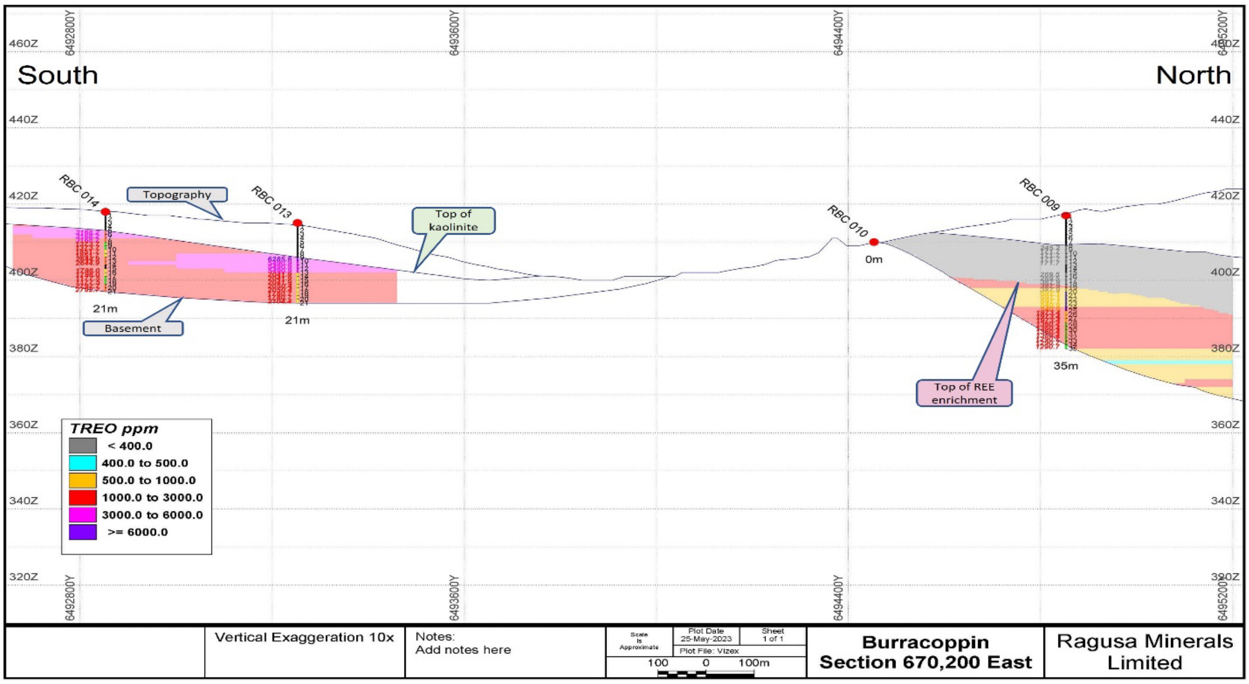


*Figure 11. Burracoppin Project – Section 670, 200 East Total Rare Earth Oxide content*

**RESOURCE SUMMARY**

**Project Geology**

The Burracoppin Project area can be described as having gently undulating surface topography with occasional low outcrop of weathered granite as an exposure of the underlying basement granite. The majority of the area consists of shallow surface soils +/- residual surface lateritisation (colluvium) in parts between 0 – 2m thick. Surface sediments blend into saprolitc clays typically between 0m and 10m thick overlying a kaolinitic unit that eventually grades into decomposed granite (as a precursor to the kaolinite) above a fresh granite basement.

Kaolinite is a weathering product of the underlying granite where the majority of the feldspar +/- mica within the original granite has become altered into kaolin but the rock retains the original quartz +/- minor accessory mineral content. The resultant kaolinite is a rock comprised predominantly of kaolin clay and residual quartz fragments from the original granite often in a ~50:50 ratio. In the case of the Burracoppin deposit, some of the kaolin has subsequently become dehydrated to form halloysite where the flat plates of kaolin have been rolled into cylindrical nanotubes. This material is a highly sought after nano particle due to its significantly increased particle surface area for use in nanotechnology, carbon capture, hydrogen storage, renewable energy, fine porcelain, etc.

Rare earth elements (REE) are also found to have been mobilized from the underlying granite and concentrated within the kaolinite zone above through either adsorption onto the clay particles or entrained within. The elevated REE grades (as high as >0.5% total REE in this data set) are typically in the lower section of the kaolinite zone immediately above the decomposed granite basement. The REE content reported in this resource only reflects the -45ųm size fraction. It is unknown if the REE grades continue through all size fractions.

**Drilling**

Air core drilling using a Toyota Landcruiser mounted Mantis drill rig was used to drill holes on 400m intervals both along lines (north – south orientation) and between lines in an offset diamond pattern. Holes were drilled vertically using an approximate 3 inch diameter blade drill bit with entire samples collected at 1m intervals into green plastic sample bags. Drill holes ranged between 1m and 35m deep averaging 13.6m across the project area and were designed to terminate at the granite basement interface.

A total of 63 holes and 1,143m were drilled.

Drill holes were located using hand held GPS with a +/- 5m accuracy in the horizontal plane. Vertical accuracy is far worse and was not relied upon for the estimation. Given the effective 400m x 400m grid pattern, the inferred category of the estimated resource and the flat lying non directional style of mineralisation, the Competent Person considers any locational discrepancy of drill hole collars to be insignificant and will not have a material effect on the overall resource.

**Sampling**

Entire 1m samples were collected from the base of the cyclone during drilling and placed in sequential order in numbered green plastic sample bags in rows of 10. Each sample was logged in the field by field technician for colour, lithology, sample recovery etc and a subsample was retained in chip trays.

Composite samples were subsequently designed after review of the logging information and inspection of the individual chipped samples and were based primarily on colour changes downhole. Composite widths averaged 3m and ranged from 1m to 6m. Samples were collected in the field with a piece of PVC pipe using a spearing technique from the top of the sample through to the bottom of the sample in a diagonal fashion. One spear was collected for each sample selected as part of the relative composite for equal representivity, and placed into a labelled fine weave calico sample bag for submission to the laboratory.

Samples logged as kaolinite totalled 553 from which 198 composite samples were collected. A subset of composite samples totalling 147 from 37 holes were then selected based on mineralized thickness and lateral kaolinite continuity between holes. These samples were used in the resource estimation and the resource boundary was adjusted accordingly. As a result, a percentage of the area remains containing known mineralisation (based on logged kaolinite) that has not been included in the estimation. Refer Tables 3, 4 and 5 for the composite assays.

**Laboratory Analysis**

Samples were delivered to the Bureau Veritas (BV) Laboratory in Canning Vale, Perth personally by the company geologist, then sent internally to the BV facility for analysis.

Sample preparation steps conducted on each sample were:

1. Dry, weigh and Stage Crush to -6.3mm on receival.
2. Weigh and riffle split a sub sample approximately 750g.

Sample Sizing:

1. Blunge using an Agitair flotation cell to agitate at ~55-60% solids 800 rpm for 15 minutes.
2. Wet screen sample at +180µm, -180ɥm, +45µm and -45ɥm.
3. Filter, dry, retain and weigh each fraction.
4. Report results.

Analysis Test Work:

1. Riffle split the -45ɥm fraction into 4 aliquots.
2. ISO-Brightness testing on the -45µm fractions
3. X-Ray Fluorescence (XRF) for: Fe2O3, SiO2, Al2O3, CaO, K2O, Mn, Na2O, MgO, P, S, TiO2, Cl and LOI.
4. ICP MS analysis using a Lithium Borate Fusion for: Ce, La, Y, Dy, Er, Eu, Gd, Ho, Lu, Nd, Pr, Sm, Tb, Tm and Yb.
5. X- Ray Diffraction (XRF) to quantify kaloinite, halloysite and other clay minerals.

**DATA**

**Drillhole Data**

Separate drill hole collar and assay files were imported as excel spreadsheets into Micromine. Data in the assay file was first de-composited into 1m intervals, then combined with the collar information in the creation of a drill hole database for use in estimation.

**Zone Wireframes**

Mineralisation is considered to be in a relatively flat lying deposit with an undulating contact with both basement and topography due to the nature of meteoric weathering in the formation of the regolith profile. The erosional surface has exposed areas of granitic outcrop considered to be expressions of the basement lithology in the area.

As such, modelling was based on an interpreted semi continuous body in all lateral directions with no particular strike or dip. The kaolinized clay zone was considered the mineralized zone for interpolation of assay data.

A basement wireframe was developed from digitized sectional strings with points snapped to logged basement intersections in each drill hole. Sectional strings were contained within a lateral boundary string and subsequently used to create a digital terrain model (DTM) of the basement interface layer. Samples (if any) beneath this layer were zoned 0 and considered as basement. This data was not used for interpolation.

Topographic data was extracted from the Copernicus GLO 30 Digital Elevation Model for the Burracoppin project area. The data packet was contoured in QGIS and exported to Micromine as contour strings. The contour strings were restricted within an external boundary string and a DTM was created of the topographical surface. The Copernicus DEM has a 30m pixel resolution and a reported relative vertical accuracy of <2m for slopes below or equal to 20%. The competent person considers this level of accuracy appropriate for this level of estimation and resource categorization. Drill hole samples beneath this layer were zoned 2 reflecting overburden.

The top of mineralisation wireframe was created in the same fashion as the basement wireframe. Sectional strings were digitized by snapping to points at the top of the first logged kaolinite sample in each drill hole. Sectional strings were restricted within a lateral boundary string for the project area and used to create a DTM of the top of mineralisation. Drill hole samples beneath the top of mineralisation surface and above the basement layer were zoned 1 to be used in interpolation of mineralisation. Halloysite distribution within the kaolinite showed no particular spatial preference so no attempt was made to isolate for its separate interpolation.

Interpretation of the REE data revealed a consistent zone within the broader mineralisation of REE enrichment in the lower section of the kaolinite. Using a TREO cut-off of 400ppm, sectional strings were digitized by snapping to the relevant point in each drill hole as an upper layer. A lateral boundary string was created and used in conjunction with the sectional strings to create a DTM of the upper surface of REE enrichment. Drill hole samples between the upper REE surface and the base of kaolinite mineralisation were re-zoned 21 as a subset of zone 1 for the purposes of REE interpolation only.

**Data Zoning**

Samples in the drill hole database were assigned a zone number using the zone wireframes to correspond with the respective zone number in the prototype block model. This zone number was used to determine which samples applied to which zone during the interpolation.

**RESOURCE ESTIMATION**

**Zone Modelling**

Model Prototype Construction

A model prototype was constructed within a lateral area boundary using the wireframes described in the previous section. Cells were constructed using a parent size of 100m in the X direction, 100m in the Y direction and 1m in the Z direction with the model orientated north – south. Sub cells were created along zone boundaries to a minimum of 10m in the X direction, 10m in the Y direction and 0.5m in the Z direction if required to reflect the variable nature of zone interfaces. From top down, the following zone numbers were allocated to the prototype model coincident with the zoning applied to the drill hole data set:

- From topographical surface down: 2
- From top of mineralisation down: 1
- From top of REE 400ppm cut-off down: 21
- From basement down: 0

No internal waste was defined in this model.

The final prototype model was cut to the drill holes used in the estimation and to within the lease boundary (E70/5708).

**Estimation Methodology**

Both Ordinary Kriging (OK) and Inverse Distance (ID) interpolation methods were investigated for use in the estimation. Variograms were created for several representative variables and trial interpolation was conducted with OK. A similar approach was taken using ID for the same variables and comparisons made for representativity and smoothing against drill hole data. Results of OK were considered overly smoothed and not satisfactorily reflective of the hard data in the drill holes in their immediate vicinity due to the widely spaced and limited data further restricted by down hole compositing.

The ID method was chosen due to its better interpolation performance against real data. Estimation was conducted systematically in three stages with wider or less onerous search parameters with the objective of the third search filling any remaining empty cells from previous searches. A description of search characteristics is as follows:

1. Rare Earth Element Variables

SEARCH 1

- Model filter: Ore = 21
- Data filter: Ore = 21
- Fields: La2O3, CeO2, Pr6O11, Nd2O3, Sm2O3, Dy2O3, Tb4O7, Y2O3, TREO
- ID power: 2
- Search geometry: Ellipsiod
- Axis Orientation: Geological plunge, west sense
- Strike: 0
- Dip: 0
- X radius: 450
- Y radius: 450
- Z radius: 4
- Number of sectors: 4
- Maximum samples per sector: 18
- Minimum total samples: 4
- Search Identification: REO_S = 1

SEARCH 2 - Same as above except for:

- Model filter: Ore = 21, REO_S = 100
- Z radius: 10
- Search Identification: REO_S = 2

SEARCH 3 - Same as above except for:

| | |
|---|---|
| - Model filter: | Ore = 21, REO_S = 100 |
| - Minimum total samples: | 2 |
| - X radius: | 900 |
| - Y radius: | 900 |
| - Z radius: | 20 |
| - Search Identification: | REO_S = 3 |

2. Low Grade Rare Earth Element Variables

SEARCH 1 (single search only)

| | |
|---|---|
| - Model filter: | 1 |
| - Data filter: | Ore = 1 |
| - Fields: | La2O3, CeO2, Pr6O11, Nd2O3, Sm2O3, Dy2O3, Tb4O7, Y2O3, TREO |
| - ID power: | 2 |
| - Search geometry: | Ellipsiod |
| - Axis Orientation: | Geological plunge, west sense |
| - Strike: | 0 |
| - Dip: | 0 |
| - X radius: | 900 |
| - Y radius: | 900 |
| - Z radius: | 20 |
| - Number of sectors: | 4 |
| - Maximum samples per sector: | 18 |
| - Minimum total samples: | 2 |
| - Search Identification: | REO_S = 4 |

3. Clay Variables

SEARCH 1

| | |
|---|---|
| - Model filter: | Ore = 21 or 1 |
| - Data filter: | Ore = 21 or 1 |
| - Fields: | -45ųm, ISO-B, Al2O3, Fe2O3, SiO2, TiO2. |
| - ID power: | 2 |
| - Search geometry: | Ellipsiod |
| - Axis Orientation: | Geological plunge, west sense |
| - Strike: | 0 |
| - Dip: | 0 |
| - X radius: | 450 |
| - Y radius: | 450 |
| - Z radius: | 5 |
| - Number of sectors: | 4 |
| - Maximum samples per sector: | 18 |
| - Minimum total samples: | 4 |
| - Search Identification: | CLY_S = 1 |

SEARCH 2 - Same as above except for:

- Model filter: CLY_S = 100
- Z radius: 10
- Search Identification: CLY_S = 2

SEARCH 3 - Same as above except for:

- Model filter: CLY_S = 100
- Minimum total samples: 2
- X radius: 900
- Y radius: 900
- Z radius: 20
- Search Identification: CLY_S = 3

4. Halloysite

SEARCH 1

- Model filter: Ore = 21 or 1
- Data filter: Ore ≠ 2 or 0
- Missing data treatment: 0
- Fields: Halloysite
- ID power: 3
- Search geometry: Ellipsiod
- Axis Orientation: Geological plunge, west sense
- Strike: 0
- Dip: 0
- X radius: 350
- Y radius: 350
- Z radius: 3
- Number of sectors: 4
- Maximum samples per sector: 18
- Minimum total samples: 2
- Search Identification: HAL_S = 1

SEARCH 2 - Same as above except for:

- Model filter: Ore ≠ 2 or 0, HAL_S = 100
- X radius: 600
- Y radius: 600
- Z radius: 4
- Search Identification: HAL_S = 2

SEARCH 3 - Same as above except for:

- Model filter: Ore ≠ 2 or 0, HAL_S = 100
- Minimum total samples: 2
- X radius: 900
- Y radius: 900

- Z radius: 20
- Search Identification: HAL_S = 3

5. Kaolinite

SEARCH 1

- Model filter: Ore = 21 or 1
- Data filter: Ore ≠ 2 or 0
- Missing data treatment: Ignored
- Fields: Kaolinite
- ID power: 2
- Search geometry: Ellipsiod
- Axis Orientation: Geological plunge, west sense
- Strike : 0
- Dip: 0
- X radius: 450
- Y radius: 450
- Z radius: 4
- Number of sectors: 4
- Maximum samples per sector: 18
- Minimum total samples: 4
- Search Identification: MIN_S = 1

SEARCH 2 - Same as above except for:

- Model filter: MIN_S = 100
- X radius: 450
- Y radius: 450
- Z radius: 10
- Search Identification: MIN_S = 2

SEARCH 3 - Same as above except for:

- Model filter: MIN_S = 100
- Minimum total samples: 2
- X radius: 900
- Y radius: 900
- Z radius: 20
- Search Identification: MIN_S = 3

A thorough review of the complete model was conducted with results deemed satisfactory for the models inferred level of confidence. A uniform bulk density of 1.53 g/cm3 was applied to the estimated mineralized zones as in-situ dry bulk density. This figure was derived from the neighbouring project which lies directly adjacent to the Burracoppin project on its eastern side. The neighbouring project assumed the value of 1.53 g/cm3 based on similar kaolinized granite deposits in Australia, with values ranging from 1.4 g/cm3 - 1.9 g/cm3.

**RESOURCE CLASSIFICATION**

The resource in its entirety has been categorised as Inferred in accordance with the JORC Code (2012). Drilling density is wide spaced and although variography indicated data ranges between 800m and 1,200m, it was considered this was a function of the limited data set in the first instance. The inherent geology suggests a high degree of uniformity from an elemental and kaolinite content perspective however the same cannot be said for the formation of halloysite and to a similar degree, REE mineralisation. This is due to the poorly understood influences and causes of dehydration and resultant levels of alteration of kaolinite as the precursor to halloysite formation.

Future work should include closer spaced drilling and preferably smaller and more consistent compositing of samples. A greater data set will improve the variography and possibly lend itself to better performance using ordinary kriging as an estimation method.

A global cut-off grade of >70 ISO-B was applied in the reporting of the resource for clay variables, halloysite and kaolinite. No additional cut-off was applied to halloysite as it is a co-product of mining kaolinite and would not, not be mined below any arbitrary cut-off.

A cut-off grade of >400ppm TREO was applied to the interpretation and reporting of REO mineralisation. This was sourced from similar REO projects reported in Australia with cut-off grades ranging between 300ppm TREO and 500ppm TREO. There is also quite a distinct break in mineralisation at that level in the assay data.

**ENDS**

*This announcement has been authorised by Jerko Zuvela, the Company's Chair.*

*For more information on Ragusa Minerals Limited and to subscribe for regular updates, please visit our website at www.ragusaminerals.com.au or contact us via admin@ragusaminerals.com.au.*

**For further information:**

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Chair

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**Reference to Previous ASX Releases:**
This document refers to the following third party ASX releases:
31st May 2021 – Latin Resources Ltd (ASX: LRS), 207Mt Maiden Inferred (JORC 2012) Mineral Resource Estimate Noombenberry Kaolin-Halloysite Project, WA

Ragusa confirms that it is not aware of any new information or data that materially affects the information included in the original market announcement and, in the case of Mineral Resources or Ore Reserves, that all material assumptions and technical parameters underpinning the estimates in the relevant market announcement continue to apply and have not materially changed. Ragusa confirms that the form and context in which the Competent Person's findings are presented have not been materially modified from the original market announcement.

**Forward Looking Statements:** Statements regarding plans with respect to the Company's mineral properties are forward looking statements. There can be no assurance that the Company's plans for development of its mineral properties will proceed as expected. There can be no assurance that the Company will be able to confirm the presence of mineral deposits, that any mineralisation will prove to be economic or that a mine will successfully be developed on any of the Company's mineral properties.

**Competent Person's Statement**

*The information contained in this ASX release relating to Exploration Results has been reviewed by Mr Olaf Frederickson. Mr Frederickson is a Member of the Australasian Institute of Mining and Metallurgy and has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves. Mr Frederickson is an Executive Director of Ragusa Minerals Ltd and consents to the inclusion in this announcement of this information in the form and context in which it appears.*

## ABOUT RAGUSA MINERALS LIMITED

Ragusa Minerals Limited (ASX: RAS) is an Australian company with an interest in the following projects – NT Lithium Project (including Litchfield and Daly River Lithium Projects) in Northern Territory, Monte Cristo Gold Project in Alaska, Burracoppin Halloysite Project in Western Australia, and Lonely Mine Gold Project in Zimbabwe.

The Company has an experienced board and management team with a history of exploration, operational and corporate success.

Ragusa leverages the team's energy, technical and commercial acumen to execute the Company's mission - to maximize shareholder value through focussed, data-driven, risk-weighted exploration and development of our assets.

***Table 3. Drillhole Collar Information***

| Hole ID | Easting | Northing | RL | Dip | Azimuth | Total Depth |
|---|---|---|---|---|---|---|
| RBC 001 | 670626 | 6495053 | 429 | -90 | 360 | 20 |
| RBC 002 | 670626 | 6494653 | 425 | -90 | 360 | 29 |
| RBC 003 | 670625 | 6494323 | 417 | -90 | 360 | 11 |
| RBC 004 | 670618 | 6493872 | 408 | -90 | 360 | 9 |
| RBC 005 | 670604 | 6493454 | 410 | -90 | 360 | 8 |
| RBC 006 | 670593 | 6493054 | 424 | -90 | 360 | 14 |
| RBC 007 | 670589 | 6492654 | 425 | -90 | 360 | 19 |
| RBC 008 | 670574 | 6492254 | 421 | -90 | 360 | 21 |
| RBC 009 | 670174 | 6494853 | 421 | -90 | 360 | 35 |
| RBC 010 | 670226 | 6494453 | 414 | -90 | 360 | 0.1 |
| RBC 011 | 670226 | 6494053 | 405 | -90 | 360 | 0.1 |
| RBC 012 | 670226 | 6493653 | 409 | -90 | 360 | 9 |
| RBC 013 | 670226 | 6493253 | 418 | -90 | 360 | 21 |
| RBC 014 | 670226 | 6492853 | 421 | -90 | 360 | 21 |
| RBC 015 | 670226 | 6492453 | 422 | -90 | 360 | 5 |
| RBC 016 | 670226 | 6492053 | 421 | -90 | 360 | 0.1 |
| RBC 017 | 669826 | 6495053 | 424 | -90 | 360 | 25 |
| RBC 018 | 669826 | 6494653 | 419 | -90 | 360 | 35 |
| RBC 019 | 669826 | 6494253 | 411 | -90 | 360 | 0.1 |
| RBC 020 | 669826 | 6493853 | 403 | -90 | 360 | 9 |
| RBC 021 | 669826 | 6493453 | 405 | -90 | 360 | 21 |
| RBC 022 | 669826 | 6493053 | 414 | -90 | 360 | 0.1 |
| RBC 023 | 669826 | 6492653 | 418 | -90 | 360 | 0.1 |
| RBC 024 | 669826 | 6492253 | 418 | -90 | 360 | 0.1 |
| RBC 025 | 669426 | 6494853 | 415 | -90 | 360 | 25 |
| RBC 026 | 669426 | 6494453 | 414 | -90 | 360 | 0.1 |
| RBC 027 | 669426 | 6494053 | 405 | -90 | 360 | 0.1 |
| RBC 028 | 669426 | 6493653 | 398 | -90 | 360 | 21 |
| RBC 029 | 669426 | 6493253 | 408 | -90 | 360 | 0.1 |
| RBC 030 | 669426 | 6492853 | 411 | -90 | 360 | 0.1 |
| RBC 031 | 669426 | 6492453 | 412 | -90 | 360 | 9 |
| RBC 032 | 669426 | 6492053 | 413 | -90 | 360 | 0.1 |
| RBC 033 | 669026 | 6495853 | 415 | -90 | 360 | 0.1 |
| RBC 034 | 669026 | 6495453 | 419 | -90 | 360 | 15 |
| RBC 035 | 669026 | 6495053 | 414 | -90 | 360 | 18 |

| | | | | | | |
|---|---|---|---|---|---|---|
| RBC 036 | 669026 | 6494653 | 408 | -90 | 360 | 0.1 |
| RBC 037 | 669026 | 6494253 | 406 | -90 | 360 | 22 |
| RBC 038 | 669026 | 6493853 | 399 | -90 | 360 | 23 |
| RBC 039 | 669026 | 6493453 | 399 | -90 | 360 | 19 |
| RBC 040 | 669026 | 6493053 | 401 | -90 | 360 | 0.1 |
| RBC 041 | 669026 | 6492653 | 407 | -90 | 360 | 20 |
| RBC 042 | 669026 | 6492253 | 410 | -90 | 360 | 22 |
| RBC 043 | 668626 | 6496053 | 410 | -90 | 360 | 10 |
| RBC 044 | 668626 | 6495653 | 421 | -90 | 360 | 10 |
| RBC 045 | 668626 | 6495253 | 417 | -90 | 360 | 18 |
| RBC 046 | 668626 | 6494853 | 406 | -90 | 360 | 9 |
| RBC 047 | 668626 | 6494453 | 402 | -90 | 360 | 22 |
| RBC 048 | 668626 | 6494053 | 397 | -90 | 360 | 19 |
| RBC 049 | 668626 | 6493653 | 395 | -90 | 360 | 12 |
| RBC 050 | 668626 | 6493253 | 401 | -90 | 360 | 13 |
| RBC 051 | 668626 | 6492853 | 409 | -90 | 360 | 28 |
| RBC 052 | 668626 | 6492453 | 411 | -90 | 360 | 28 |
| RBC 053 | 668626 | 6492053 | 416 | -90 | 360 | 26 |
| RBC 054 | 668226 | 6495853 | 411 | -90 | 360 | 17 |
| RBC 055 | 668226 | 6495453 | 417 | -90 | 360 | 16 |
| RBC 056 | 668226 | 6495053 | 411 | -90 | 360 | 0.1 |
| RBC 057 | 668226 | 6494653 | 401 | -90 | 360 | 23 |
| RBC 058 | 668226 | 6494253 | 394 | -90 | 360 | 20 |
| RBC 059 | 668226 | 6493853 | 394 | -90 | 360 | 0.1 |
| RBC 060 | 668226 | 6493453 | 402 | -90 | 360 | 26 |
| RBC 061 | 668226 | 6493053 | 408 | -90 | 360 | 31 |
| RBC 062 | 668226 | 6492653 | 416 | -90 | 360 | 12 |
| RBC 063 | 668226 | 6492253 | 422 | -90 | 360 | 11 |

***Table 4. Rare Earth Element assay results***

| HOLE ID | Depth | | Sample | | -45µm | La | Ce | Pr | Nd | Sm | Dy | Tb | Y | TREO |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | From m | To m | ID | Interval | % | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) | (ppm) |
| RBC 001 | 6 | 8 | 01_1 | 2 | 48.1 | 47 | 86.5 | 8 | 26 | 4.5 | 1.5 | <0.5 | 5 | 218 |
| RBC 001 | 8 | 13 | 01_2 | 5 | 50.0 | 83 | 144 | 14 | 40.5 | 5.5 | 2.5 | 0.5 | 7 | 362 |
| RBC 001 | 13 | 15 | 01_3 | 2 | 46.5 | 162 | 253 | 22 | 69 | 9 | 3 | 1 | 10 | 644 |
| RBC 001 | 15 | 16 | 01_4 | 1 | 45.8 | 172 | 281 | 26 | 76 | 10.5 | 3 | 1 | 11 | 709 |
| RBC 001 | 16 | 19 | 01_5 | 3 | 40.2 | 210 | 344 | 30 | 89.5 | 11 | 3.5 | 1 | 12 | 854 |
| RBC 001 | 19 | 20 | 01_6 | 1 | 42.8 | 377 | 516 | 44 | 118 | 14 | 4.5 | 1 | 14 | 1322 |
| RBC 002 | 14 | 17 | 02_1 | 3 | 52.3 | 728 | 1260 | 12 | 392 | 47.5 | 13 | 3 | 38 | 3186 |
| RBC 002 | 17 | 20 | 02_2 | 3 | 50.8 | 752 | 1380 | 13 | 402 | 46 | 16 | 3.5 | 59 | 3415 |
| RBC 002 | 20 | 22 | 02_3 | 2 | 52.5 | 524 | 1100 | 11 | 427 | 63 | 34 | 7.5 | 128 | 3011 |
| RBC 002 | 22 | 23 | 02_4 | 1 | 50.9 | 234 | 493 | 54 | 188 | 27.5 | 16.5 | 3.5 | 58 | 1347 |
| RBC 002 | 23 | 27 | 02_5 | 4 | 45.7 | 221 | 475 | 52 | 186 | 27 | 17.5 | 4 | 76 | 1333 |
| RBC 002 | 27 | 29 | 02_6 | 2 | 25.8 | 201 | 410 | 46 | 160 | 21.5 | 10.5 | 2 | 57 | 1134 |
| RBC 006 | 4 | 8 | 06_1 | 4 | 50.8 | 16 | 23 | 2 | 7 | 1.5 | 1 | <0.5 | 3 | 65 |
| RBC 006 | 8 | 12 | 06_2 | 4 | 45.9 | 25 | 39.5 | 4 | 11.5 | 2.5 | 1 | <0.5 | 5 | 109 |
| RBC 006 | 12 | 13 | 06_3 | 1 | 30.5 | 94 | 158 | 18 | 51 | 7.5 | 3 | 0.5 | 14 | 428 |
| RBC 006 | 13 | 14 | 06_4 | 1 | 20.5 | 71 | 127 | 14 | 42 | 5.5 | 3.5 | 0.5 | 13 | 344 |
| RBC 007 | 4 | 8 | 07_1 | 4 | 55.5 | 19 | 33 | 4 | 10.5 | 1.5 | 1 | <0.5 | 4 | 90 |
| RBC 007 | 8 | 12 | 07_2 | 4 | 57.3 | 51 | 97 | 10 | 32.5 | 5 | 2.5 | 0.5 | 9 | 255 |
| RBC 007 | 12 | 16 | 07_3 | 4 | 53.7 | 59 | 108 | 12 | 37.5 | 6 | 3 | 0.5 | 10 | 291 |
| RBC 007 | 16 | 19 | 07_4 | 3 | 39.4 | 114 | 200 | 18 | 61 | 10 | 4 | 1 | 16 | 522 |
| RBC 008 | 7 | 11 | 08_1 | 4 | 53.1 | 39 | 70.5 | 8 | 23 | 4 | 2.5 | <0.5 | 9 | 192 |
| RBC 008 | 11 | 15 | 08_2 | 4 | 54.6 | 51 | 91.5 | 10 | 31 | 5 | 2.5 | 0.5 | 9 | 247 |

| | | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| RBC 008 | 15 | 19 | 08_3 | 4 | 44.5 | 73 | 118 | 12 | 36.5 | 6 | 3 | 0.5 | 10 | 318 |
| RBC 008 | 19 | 21 | 08_4 | 2 | 35.9 | 174 | 257 | 24 | 72.5 | 10.5 | 4.5 | 1 | 18 | 689 |
| RBC 009 | 8 | 9 | 09_1 | 1 | 30.5 | 68 | 84 | 10 | 27 | 4 | 1.5 | <0.5 | 7 | 245 |
| RBC 009 | 9 | 13 | 09_2 | 4 | 57.9 | 41 | 66 | 6 | 19.5 | 3.5 | 1 | <0.5 | 4 | 172 |
| RBC 009 | 15 | 17 | 09_3 | 2 | 55.9 | 64 | 102 | 10 | 31.5 | 5 | 2 | <0.5 | 6 | 270 |
| RBC 009 | 17 | 20 | 09_4 | 3 | 46.5 | 84 | 148 | 16 | 49.5 | 7 | 3 | 0.5 | 9 | 388 |
| RBC 009 | 20 | 23 | 09_5 | 3 | 46.8 | 126 | 241 | 24 | 74 | 9.5 | 3.5 | 1 | 9 | 597 |
| RBC 009 | 23 | 25 | 09_6 | 2 | 50.4 | 121 | 212 | 20 | 64.5 | 9.5 | 3.5 | 1 | 9 | 541 |
| RBC 009 | 25 | 28 | 09_7 | 3 | 43.3 | 403 | 728 | 96 | 306 | 42.5 | 9 | 2.5 | 21 | 1973 |
| RBC 009 | 28 | 32 | 09_8 | 4 | 36.7 | 316 | 467 | 56 | 195 | 27.5 | 9.5 | 2.5 | 28 | 1360 |
| RBC 009 | 32 | 35 | 09_9 | 3 | 37.8 | 275 | 482 | 50 | 170 | 25 | 8.5 | 2 | 32 | 1291 |
| RBC 013 | 9 | 10 | 13_1 | 1 | 38.5 | 852 | 2540 | 28 | 1040 | 150 | 49 | 11 | 145 | 6286 |
| RBC 013 | 10 | 13 | 13_2 | 3 | 31.2 | 621 | 2630 | 16 | 601 | 83.5 | 43.5 | 9 | 247 | 5491 |
| RBC 013 | 13 | 16 | 13_3 | 3 | 28.9 | 357 | 709 | 80 | 292 | 41.5 | 22 | 4.5 | 121 | 2042 |
| RBC 013 | 16 | 18 | 13_4 | 2 | 28.5 | 361 | 740 | 82 | 286 | 39 | 21.5 | 4.5 | 104 | 2050 |
| RBC 013 | 18 | 20 | 13_5 | 2 | 23.7 | 301 | 622 | 72 | 265 | 39 | 20.5 | 4 | 94 | 1781 |
| RBC 013 | 20 | 21 | 13_6 | 1 | 23.3 | 397 | 739 | 80 | 291 | 40.5 | 24 | 5 | 102 | 2104 |
| RBC 014 | 5 | 8 | 14_2 | 3 | 39.8 | 608 | 1180 | 12 | 486 | 62.5 | 27.5 | 6.5 | 63 | 3168 |
| RBC 014 | 8 | 10 | 14_3 | 2 | 39.7 | 270 | 494 | 52 | 202 | 27 | 15 | 3.5 | 40 | 1374 |
| RBC 014 | 10 | 12 | 14_4 | 2 | 36.4 | 365 | 699 | 72 | 246 | 31 | 15 | 3 | 65 | 1852 |
| RBC 014 | 12 | 14 | 14_5 | 2 | 34.7 | 537 | 907 | 94 | 331 | 40.5 | 27 | 5 | 174 | 2645 |
| RBC 014 | 15 | 17 | 14_6 | 2 | 35.3 | 361 | 672 | 70 | 251 | 30.5 | 14 | 3 | 53 | 1798 |
| RBC 014 | 17 | 19 | 14_7 | 2 | 40.1 | 276 | 425 | 42 | 137 | 16.5 | 8 | 1.5 | 46 | 1178 |
| RBC 014 | 19 | 21 | 14_8 | 2 | 26.7 | 489 | 1040 | 10 | 390 | 51.5 | 23 | 5 | 133 | 2793 |
| RBC 017 | 10 | 14 | 17_1 | 4 | 52.1 | 64 | 119 | 10 | 33 | 5 | 2 | <0.5 | 6 | 291 |
| RBC 017 | 14 | 18 | 17_2 | 4 | 55.1 | 51 | 87 | 8 | 25.5 | 4 | 1.5 | <0.5 | 4 | 221 |
| RBC 017 | 18 | 20 | 17_3 | 2 | 51.2 | 85 | 131 | 12 | 41.5 | 6 | 2 | 0.5 | 9 | 351 |
| RBC 017 | 20 | 22 | 17_4 | 2 | 53.0 | 111 | 177 | 16 | 53 | 8 | 3 | 0.5 | 9 | 461 |
| RBC 017 | 22 | 24 | 17_5 | 2 | 49.5 | 131 | 227 | 20 | 66 | 10 | 3.5 | 1 | 10 | 576 |
| RBC 017 | 24 | 25 | 17-6 | 1 | 49.2 | 96 | 146 | 15 | 47 | 7.5 | 3 | 1 | 10 | 402 |
| RBC 018 | 9 | 12 | 18-1 | 3 | 44.1 | 37 | 57 | 5 | 15.5 | 3 | 1 | <0.5 | 4 | 150 |
| RBC 018 | 12 | 16 | 18-2 | 4 | 55.0 | 55 | 87 | 8 | 24 | 3.5 | 1 | <0.5 | 3 | 222 |
| RBC 018 | 16 | 20 | 18-3 | 4 | 56.1 | 37 | 54.5 | 5 | 17 | 2.5 | 1 | <0.5 | 3 | 146 |
| RBC 018 | 20 | 22 | 18-4 | 2 | 56.1 | 42 | 61.5 | 5 | 18 | 3 | 1 | <0.5 | 3 | 163 |
| RBC 018 | 22 | 26 | 18-5 | 4 | 52.5 | 92 | 154 | 14 | 45.5 | 6.5 | 2.5 | 0.5 | 7 | 393 |
| RBC 018 | 26 | 30 | 18-6 | 4 | 45.9 | 124 | 221 | 22 | 71.5 | 11.5 | 5 | 1 | 23 | 593 |
| RBC 018 | 30 | 35 | 18-7 | 5 | 43.0 | 114 | 182 | 18 | 57 | 8.5 | 3 | 0.5 | 12 | 487 |
| RBC 020 | 3 | 6 | 20-1 | 3 | 47.3 | 199 | 260 | 22 | 68.5 | 9 | 4 | 1 | 18 | 713 |
| RBC 020 | 6 | 9 | 20-2 | 3 | 34.4 | 436 | 564 | 42 | 116 | 12.5 | 4 | 1 | 14 | 1443 |
| RBC 021 | 14 | 15 | 21-2 | 1 | 36.3 | 176 | 355 | 38 | 124 | 17.5 | 7.5 | 1.5 | 34 | 932 |
| RBC 021 | 15 | 21 | 21-3 | 6 | 28.2 | 651 | 1400 | 15 | 574 | 88 | 39 | 8.5 | 151 | 3833 |
| RBC 025 | 8 | 11 | 25-1 | 3 | 53.7 | 99 | 147 | 14 | 42.5 | 5.5 | 2 | <0.5 | 6 | 387 |
| RBC 025 | 11 | 15 | 25-2 | 4 | 50.3 | 54 | 82 | 8 | 26 | 4 | 1.5 | <0.5 | 5 | 220 |
| RBC 025 | 15 | 18 | 25-3 | 3 | 49.0 | 94 | 146 | 15 | 47.5 | 6.5 | 2 | <0.5 | 10 | 391 |
| RBC 025 | 18 | 20 | 25-4 | 2 | 44.4 | 196 | 318 | 32 | 103 | 14.5 | 4.5 | 1 | 16 | 841 |
| RBC 025 | 20 | 23 | 25-5 | 3 | 43.9 | 220 | 375 | 39 | 136 | 20 | 6 | 1.5 | 28 | 1018 |
| RBC 025 | 23 | 25 | 25-6 | 2 | 41.6 | 176 | 307 | 33 | 110 | 15 | 4.5 | 1 | 22 | 822 |
| RBC 028 | 5 | 7 | 28-1 | 2 | 35.1 | 38 | 45 | 4 | 13 | 2 | 1 | <0.5 | 3 | 129 |
| RBC 028 | 7 | 12 | 28-2 | 5 | 46.7 | 58 | 84.5 | 8 | 24.5 | 3.5 | 1.5 | <0.5 | 6 | 227 |
| RBC 028 | 12 | 14 | 28-3 | 2 | 48.3 | 60 | 91 | 11 | 34 | 4.5 | 2 | <0.5 | 9 | 262 |
| RBC 028 | 14 | 18 | 28-4 | 4 | 45.4 | 167 | 739 | 38 | 117 | 17 | 6.5 | 1.5 | 28 | 1376 |
| RBC 028 | 18 | 21 | 28-5 | 3 | 36.8 | 1120 | 1760 | 19 | 651 | 92 | 35 | 7.5 | 164 | 4982 |
| RBC 034 | 4 | 6 | 34-1 | 2 | 39.7 | 21 | 35.5 | 3 | 11 | 2 | 0.5 | <0.5 | 2 | 91 |
| RBC 034 | 6 | 8 | 34-2 | 2 | 45.2 | 34 | 61 | 5 | 19 | 3 | 1 | <0.5 | 3 | 154 |
| RBC 034 | 8 | 11 | 34-3 | 3 | 43.5 | 142 | 244 | 24 | 75.5 | 9.5 | 2.5 | 0.5 | 8 | 617 |

| | | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| RBC 034 | 11 | 13 | 34-4 | 2 | 39.4 | 189 | 320 | 31 | 97 | 12 | 3 | 1 | 11 | 812 |
| RBC 034 | 13 | 15 | 34-5 | 2 | 38.1 | 153 | 267 | 25 | 72.5 | 10 | 2.5 | 0.5 | 10 | 661 |
| RBC 035 | 4 | 10 | 35-1 | 6 | 50.7 | 49 | 79.5 | 8 | 26 | 3.5 | 1.5 | <0.5 | 6 | 212 |
| RBC 035 | 10 | 11 | 35-2 | 1 | 46.6 | 86 | 128 | 13 | 42.5 | 5.5 | 2 | 0.5 | 8 | 350 |
| RBC 035 | 11 | 12 | 35-3 | 1 | 45.8 | 156 | 259 | 26 | 85.5 | 11.5 | 4.5 | 1 | 20 | 695 |
| RBC 035 | 12 | 14 | 35-4 | 2 | 43.2 | 120 | 187 | 19 | 58.5 | 8.5 | 2.5 | 0.5 | 11 | 500 |
| RBC 035 | 14 | 16 | 35-5 | 2 | 31.3 | 136 | 220 | 22 | 68 | 9 | 3.5 | 0.5 | 11 | 576 |
| RBC 037 | 5 | 8 | 37-1 | 3 | 47.8 | 3 | 6.5 | <1 | 1.5 | 0.5 | <0.5 | <0.5 | 1 | 15 |
| RBC 037 | 9 | 12 | 37-2 | 3 | 55.9 | 6 | 11.5 | 1 | 3.5 | 1 | <0.5 | <0.5 | 1 | 29 |
| RBC 037 | 13 | 17 | 37-3 | 4 | 56.5 | 41 | 74.5 | 7 | 25 | 4 | 1.5 | <0.5 | 5 | 194 |
| RBC 037 | 20 | 22 | 37-4 | 2 | 45.3 | 153 | 291 | 32 | 103 | 13.5 | 4.5 | 1 | 13 | 751 |
| RBC 038 | 5 | 8 | 38-1 | 3 | 50.6 | 110 | 88 | 12 | 30 | 3.5 | 1.5 | <0.5 | 5 | 303 |
| RBC 038 | 8 | 10 | 38-2 | 2 | 51.6 | 161 | 146 | 17 | 43 | 5 | 2 | <0.5 | 5 | 458 |
| RBC 038 | 10 | 13 | 38-3 | 3 | 50.6 | 120 | 143 | 12 | 33.5 | 4 | 2 | <0.5 | 5 | 388 |
| RBC 038 | 15 | 17 | 38-4 | 2 | 54.7 | 99 | 119 | 14 | 46 | 6 | 2.5 | <0.5 | 9 | 362 |
| RBC 038 | 17 | 21 | 38-5 | 4 | 48.2 | 141 | 232 | 24 | 82.5 | 12.5 | 5 | 1 | 24 | 646 |
| RBC 038 | 21 | 23 | 38-6 | 2 | 42.0 | 160 | 243 | 24 | 77.5 | 11.5 | 5 | 1 | 23 | 672 |
| RBC 039 | 9 | 11 | 39-1 | 2 | 48.4 | 24 | 38.5 | 3 | 12 | 2 | 1 | <0.5 | 4 | 104 |
| RBC 039 | 11 | 13 | 39-2 | 2 | 49.3 | 65 | 101 | 11 | 34 | 5 | 2 | <0.5 | 8 | 278 |
| RBC 039 | 14 | 16 | 39-3 | 2 | 45.6 | 171 | 271 | 29 | 90.5 | 12.5 | 4.5 | 1 | 18 | 735 |
| RBC 039 | 16 | 19 | 39-4 | 3 | 32.7 | 176 | 303 | 31 | 91.5 | 12 | 4.5 | 1 | 21 | 788 |
| RBC 045 | 5 | 9 | 45-1 | 4 | 49.1 | 37 | 65.5 | 6 | 23 | 3.5 | 1.5 | <0.5 | 5 | 174 |
| RBC 045 | 9 | 13 | 45-2 | 4 | 50.8 | 53 | 91 | 10 | 30 | 4.5 | 1.5 | <0.5 | 6 | 239 |
| RBC 045 | 13 | 15 | 45-3 | 2 | 53.4 | 74 | 127 | 13 | 41 | 6 | 1.5 | <0.5 | 6 | 327 |
| RBC 045 | 15 | 18 | 45-4 | 3 | 38.8 | 85 | 144 | 14 | 44.5 | 6.5 | 2 | <0.5 | 8 | 370 |
| RBC 046 | 6 | 7 | 46-1 | 1 | 17.3 | 16 | 23 | 2 | 8 | 1 | 0.5 | <0.5 | 3 | 64 |
| RBC 046 | 7 | 9 | 46-2 | 2 | 22.0 | 9 | 12.5 | 1 | 4.5 | 1 | 0.5 | <0.5 | 3 | 38 |
| RBC 047 | 7 | 9 | 47-1 | 2 | 53.9 | 36 | 62.5 | 6 | 20 | 3 | 0.5 | <0.5 | 3 | 160 |
| RBC 047 | 9 | 12 | 47-2 | 3 | 55.7 | 54 | 92 | 9 | 30 | 4 | 1 | <0.5 | 4 | 237 |
| RBC 047 | 12 | 18 | 47-3 | 6 | 58.7 | 74 | 135 | 14 | 44.5 | 6 | 2 | <0.5 | 8 | 346 |
| RBC 047 | 18 | 22 | 47-4 | 4 | 61.1 | 51 | 81.5 | 9 | 27.5 | 4 | 1.5 | <0.5 | 6 | 221 |
| RBC 048 | 5 | 6 | 48-1 | 1 | 48.6 | 13 | 22 | 2 | 6 | 1 | 0.5 | <0.5 | 3 | 57 |
| RBC 048 | 6 | 7 | 48-2 | 1 | 65.3 | 25 | 41 | 4 | 13 | 2 | 1 | <0.5 | 3 | 109 |
| RBC 048 | 7 | 12 | 48-3 | 5 | 64.7 | 30 | 51.5 | 5 | 16.5 | 2.5 | 1 | <0.5 | 5 | 136 |
| RBC 048 | 12 | 16 | 48-4 | 4 | 55.2 | 60 | 94.5 | 9 | 27.5 | 4.5 | 1.5 | <0.5 | 6 | 247 |
| RBC 048 | 16 | 19 | 48-5 | 3 | 39.4 | 104 | 160 | 16 | 51.5 | 6.5 | 3 | 0.5 | 13 | 435 |
| RBC 049 | 4 | 6 | 49-1 | 2 | 34.1 | 40 | 66 | 6 | 19.5 | 3 | 1.5 | <0.5 | 6 | 173 |
| RBC 049 | 6 | 12 | 49-2 | 6 | 18.8 | 13 | 16.5 | 1 | 4.5 | 0.5 | 1 | <0.5 | 5 | 50 |
| RBC 050 | 4 | 6 | 50-1 | 2 | 51.0 | 12 | 14.5 | 1 | 4 | 0.5 | <0.5 | <0.5 | 2 | 41 |
| RBC 050 | 6 | 8 | 50-2 | 2 | 71.2 | 10 | 12 | <1 | 3 | 1 | <0.5 | <0.5 | 2 | 34 |
| RBC 050 | 8 | 13 | 50-3 | 5 | 54.1 | 95 | 179 | 19 | 64 | 8.5 | 3 | 0.5 | 14 | 473 |
| RBC 057 | 6 | 7 | 57-1 | 1 | 22.5 | 17 | 50.5 | 3 | 10 | 1.5 | 1.5 | <0.5 | 7 | 111 |
| RBC 057 | 7 | 10 | 57-2 | 3 | 51.1 | 74 | 142 | 11 | 32 | 4.5 | 1 | <0.5 | 6 | 329 |
| RBC 057 | 10 | 14 | 57-3 | 4 | 56.4 | 44 | 69 | 6 | 21.5 | 3 | 1.5 | <0.5 | 6 | 185 |
| RBC 057 | 14 | 15 | 57-4 | 1 | 55.9 | 75 | 118 | 12 | 38 | 6 | 2 | <0.5 | 9 | 317 |
| RBC 057 | 15 | 17 | 57-5 | 2 | 53.2 | 37 | 55.5 | 5 | 17.5 | 3 | 1 | <0.5 | 5 | 151 |
| RBC 057 | 17 | 20 | 57-6 | 3 | 52.6 | 68 | 97.5 | 10 | 28.5 | 4.5 | 2 | <0.5 | 8 | 266 |
| RBC 057 | 20 | 23 | 57-7 | 3 | 53.3 | 60 | 93.5 | 9 | 29 | 4.5 | 2.5 | <0.5 | 11 | 257 |
| RBC 058 | 5 | 9 | 58-1 | 4 | 37.4 | 26 | 47.5 | 4 | 14.5 | 2 | 1 | <0.5 | 5 | 122 |
| RBC 058 | 9 | 12 | 58-2 | 3 | 44.0 | 39 | 74.5 | 7 | 25.5 | 4 | 1.5 | <0.5 | 7 | 194 |
| RBC 058 | 12 | 15 | 58-3 | 3 | 55.9 | 107 | 189 | 19 | 64 | 10 | 4 | 1 | 15 | 504 |
| RBC 058 | 15 | 20 | 58-4 | 5 | 43.1 | 93 | 168 | 17 | 54.5 | 7.5 | 3.5 | 0.5 | 16 | 446 |
| RBC 060 | 4 | 5 | 60-1 | 1 | 40.1 | 6 | 8 | <1 | 2.5 | 0.5 | <0.5 | <0.5 | 2 | 23 |
| RBC 060 | 5 | 8 | 60-2 | 3 | 35.1 | 5 | 7.5 | <1 | 2 | <0.5 | <0.5 | <0.5 | 2 | 20 |
| RBC 060 | 8 | 10 | 60-3 | 2 | 47.8 | 5 | 8 | <1 | 2 | <0.5 | <0.5 | <0.5 | 1 | 19 |

| | | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| RBC 060 | 10 | 13 | 60-4 | 3 | 54.8 | 36 | 61.5 | 5 | 16.5 | 2 | 0.5 | <0.5 | 3 | 152 |
| RBC 060 | 13 | 15 | 60-5 | 2 | 47.8 | 59 | 91 | 9 | 25 | 3 | 1 | <0.5 | 5 | 234 |
| RBC 060 | 15 | 20 | 60-6 | 5 | 40.5 | 125 | 206 | 19 | 56 | 6.5 | 2 | <0.5 | 7 | 512 |
| RBC 060 | 20 | 22 | 60-7 | 2 | 41.2 | 186 | 271 | 24 | 69 | 9 | 2.5 | 0.5 | 10 | 696 |
| RBC 060 | 22 | 26 | 60-8 | 4 | 44.5 | 280 | 408 | 39 | 115 | 14 | 4.5 | 1 | 21 | 1079 |
| RBC 061 | 4 | 6 | 61-2 | 2 | 53.6 | 3 | 7 | <1 | 1.5 | 0.5 | <0.5 | <0.5 | 2 | 17 |
| RBC 061 | 6 | 9 | 61-3 | 3 | 59.4 | 3 | 5.5 | <1 | 2 | 0.5 | <0.5 | <0.5 | 3 | 17 |
| RBC 061 | 9 | 11 | 61-4 | 2 | 50.1 | 9 | 17.5 | 1 | 5.5 | 1 | 0.5 | <0.5 | 5 | 48 |
| RBC 061 | 11 | 13 | 61-5 | 2 | 53.9 | 23 | 39.5 | 3 | 12 | 1.5 | 1 | <0.5 | 5 | 105 |
| RBC 061 | 13 | 16 | 61-6 | 3 | 55.1 | 32 | 54 | 5 | 17 | 3 | 1 | <0.5 | 4 | 142 |
| RBC 061 | 16 | 19 | 61-7 | 3 | 43.8 | 61 | 112 | 11 | 34 | 4.5 | 1.5 | <0.5 | 8 | 283 |
| RBC 061 | 19 | 23 | 61-8 | 4 | 36.9 | 122 | 230 | 21 | 67 | 9.5 | 3 | 0.5 | 13 | 573 |
| RBC 061 | 23 | 25 | 61-9 | 2 | 37.7 | 292 | 467 | 40 | 120 | 17.5 | 6.5 | 1.5 | 21 | 1182 |
| RBC 061 | 25 | 28 | 61-10 | 3 | 36.4 | 265 | 397 | 36 | 106 | 13.5 | 5 | 1 | 19 | 1030 |
| RBC 061 | 28 | 29 | 61-11 | 3 | 31.4 | 250 | 352 | 31 | 87 | 12 | 3.5 | 1 | 15 | 919 |

***Table 5. Complete ISO-B, XRF and XRD assay results***

| HOLE ID | Depth | | Sample | | -0.045mm | ISO-B | $Fe_2O_3$ | $Al_2O_3$ | $TiO_2$ | Halloysite | Kaolinite |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | From m | To m | ID | Interval | % | | % | % | % | % | % |
| RBC 001 | 6 | 8 | 01_1 | 2 | 48.07 | 80.5 | 0.62 | 36.3 | 0.39 | 3 | 92 |
| RBC 001 | 8 | 13 | 01_2 | 5 | 50.02 | 82.5 | 0.49 | 34.6 | 0.48 | 3 | 80 |
| RBC 001 | 13 | 15 | 01_3 | 2 | 46.47 | 80.0 | 0.69 | 33.3 | 0.48 | 10 | 67 |
| RBC 001 | 15 | 16 | 01_4 | 1 | 45.80 | 83.5 | 0.43 | 33.1 | 0.48 | 4 | 71 |
| RBC 001 | 16 | 19 | 01_5 | 3 | 40.19 | 73.5 | 0.83 | 32.4 | 0.53 | 7 | 65 |
| RBC 001 | 19 | 20 | 01_6 | 1 | 42.83 | 78.5 | 0.7 | 32.9 | 0.5 | | 76 |
| RBC 002 | 14 | 17 | 02_1 | 3 | 52.34 | 76.5 | 1.28 | 36.5 | 2.06 | | 95 |
| RBC 002 | 17 | 20 | 02_2 | 3 | 50.84 | 77.0 | 1.19 | 36 | 2.8 | | 93 |
| RBC 002 | 20 | 22 | 02_3 | 2 | 52.53 | 83.5 | 0.6 | 37.2 | 0.61 | 24 | 71 |
| RBC 002 | 22 | 23 | 02_4 | 1 | 50.94 | 80.5 | 0.74 | 37.1 | 0.55 | 40 | 57 |
| RBC 002 | 23 | 27 | 02_5 | 4 | 45.65 | 82.5 | 0.75 | 36 | 0.5 | 18 | 79 |
| RBC 002 | 27 | 29 | 02_6 | 2 | 25.83 | 74.0 | 0.81 | 26.8 | 0.47 | 12 | 55 |
| RBC 006 | 4 | 8 | 06_1 | 4 | 50.78 | 84.0 | 0.56 | 37.5 | 0.32 | | 97 |
| RBC 006 | 8 | 12 | 06_2 | 4 | 45.93 | 84.0 | 0.52 | 34.4 | 0.4 | 15 | 69 |
| RBC 006 | 12 | 13 | 06_3 | 1 | 30.49 | 71.5 | 1.67 | 30.2 | 0.39 | 12 | 55 |
| RBC 006 | 13 | 14 | 06_4 | 1 | 20.53 | 39.0 | 3.41 | 24.5 | 0.58 | 8 | 28 |
| RBC 007 | 4 | 8 | 07_1 | 4 | 55.55 | 86.0 | 0.42 | 37.9 | 0.29 | 11 | 86 |
| RBC 007 | 8 | 12 | 07_2 | 4 | 57.32 | 88.5 | 0.17 | 37.6 | 0.39 | 17 | 78 |
| RBC 007 | 12 | 16 | 07_3 | 4 | 53.68 | 87.0 | 0.39 | 34.9 | 0.38 | | 84 |
| RBC 007 | 16 | 19 | 07_4 | 3 | 39.43 | 75.0 | 0.97 | 32.3 | 0.45 | | 76 |
| RBC 008 | 7 | 11 | 08_1 | 4 | 53.07 | 84.0 | 0.62 | 36.7 | 0.38 | 1 | 96 |
| RBC 008 | 11 | 15 | 08_2 | 4 | 54.59 | 84.5 | 0.3 | 37.1 | 0.37 | 16 | 79 |
| RBC 008 | 15 | 19 | 08_3 | 4 | 44.52 | 82.5 | 0.33 | 31.8 | 0.21 | 19 | 51 |
| RBC 008 | 19 | 21 | 08_4 | 2 | 35.86 | 73.0 | 0.9 | 31.4 | 0.44 | 13 | 58 |
| RBC 009 | 8 | 9 | 09_1 | 1 | 30.53 | 60.0 | 1.31 | 33 | 0.38 | 2 | 89 |
| RBC 009 | 9 | 13 | 09_2 | 4 | 57.89 | 88.0 | 0.28 | 38.3 | 0.18 | 8 | 90 |
| RBC 009 | 15 | 17 | 09_3 | 2 | 55.94 | 87.5 | 0.26 | 38.1 | 0.29 | 5 | 92 |
| RBC 009 | 17 | 20 | 09_4 | 3 | 46.52 | 86.0 | 0.21 | 37 | 0.37 | 30 | 65 |
| RBC 009 | 20 | 23 | 09_5 | 3 | 46.83 | 81.0 | 0.71 | 31.4 | 0.34 | 13 | 58 |
| RBC 009 | 23 | 25 | 09_6 | 2 | 50.43 | 83.0 | 0.69 | 34.4 | 0.33 | | 83 |
| RBC 009 | 25 | 28 | 09_7 | 3 | 43.29 | 80.0 | 0.68 | 31.2 | 0.32 | 8 | 61 |
| RBC 009 | 28 | 32 | 09_8 | 4 | 36.65 | 76.5 | 0.95 | 32 | 0.41 | 11 | 64 |
| RBC 009 | 32 | 35 | 09_9 | 3 | 37.76 | 71.5 | 1.29 | 32.1 | 0.64 | 10 | 66 |
| RBC 013 | 9 | 10 | 13_1 | 1 | 38.46 | 75.5 | 1.19 | 30.8 | 1.93 | 13 | 75 |

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| RBC 013 | 10 | 13 | 13_2 | 3 | 31.23 | 66.5 | 0.88 | 26.8 | 2.17 | 5 | 63 |
| RBC 013 | 13 | 16 | 13_3 | 3 | 28.85 | 73.0 | 0.71 | 25.8 | 2.07 | | 63 |
| RBC 013 | 16 | 18 | 13_4 | 2 | 28.48 | 70.5 | 0.67 | 26.3 | 2.28 | 13 | 52 |
| RBC 013 | 18 | 20 | 13_5 | 2 | 23.65 | 69.0 | 0.73 | 24.9 | 2.29 | 9 | 57 |
| RBC 013 | 20 | 21 | 13_6 | 1 | 23.28 | 54.5 | 1.67 | 25.1 | 1.68 | 3 | 66 |
| RBC 014 | 5 | 8 | 14_2 | 3 | 39.82 | 72.0 | 1.04 | 33.8 | 2.9 | | 93 |
| RBC 014 | 8 | 10 | 14_3 | 2 | 39.68 | 77.5 | 1.2 | 33.4 | 2.76 | | 95 |
| RBC 014 | 10 | 12 | 14_4 | 2 | 36.40 | 68.5 | 1.05 | 31.8 | 3.34 | | 94 |
| RBC 014 | 12 | 14 | 14_5 | 2 | 34.67 | 75.0 | 0.86 | 33.8 | 2.9 | | 93 |
| RBC 014 | 15 | 17 | 14_6 | 2 | 35.27 | 76.5 | 1.51 | 31.7 | 4.11 | 13 | 75 |
| RBC 014 | 17 | 19 | 14_7 | 2 | 40.05 | 66.5 | 1.68 | 32.2 | 1.4 | | 84 |
| RBC 014 | 19 | 21 | 14_8 | 2 | 26.70 | 66.0 | 1.44 | 26.4 | 3.16 | 8 | 66 |
| RBC 017 | 10 | 14 | 17_1 | 4 | 52.12 | 83.0 | 0.63 | 37.8 | 0.3 | | 98 |
| RBC 017 | 14 | 18 | 17_2 | 4 | 55.12 | 86.0 | 0.53 | 37.8 | 0.2 | | 98 |
| RBC 017 | 18 | 20 | 17_3 | 2 | 51.24 | 86.5 | 0.37 | 38.1 | 0.33 | 11 | 86 |
| RBC 017 | 20 | 22 | 17_4 | 2 | 53.04 | 87.5 | 0.26 | 38.2 | 0.36 | 5 | 93 |
| RBC 017 | 22 | 24 | 17-5 | 2 | 49.52 | 85.5 | 0.62 | 38.1 | 0.39 | | 98 |
| RBC 017 | 24 | 25 | 17-6 | 1 | 49.17 | 84.5 | 0.6 | 37.8 | 0.43 | | 97 |
| RBC 018 | 9 | 12 | 18-1 | 3 | 44.08 | 81.0 | 0.62 | 37.1 | 0.53 | 4 | 93 |
| RBC 018 | 12 | 16 | 18-2 | 4 | 54.99 | 83.5 | 0.48 | 37.9 | 0.39 | | 98 |
| RBC 018 | 16 | 20 | 18-3 | 4 | 56.14 | 85.5 | 0.54 | 38 | 0.28 | | 98 |
| RBC 018 | 20 | 22 | 18-4 | 2 | 56.09 | 87.0 | 0.53 | 38 | 0.22 | | 98 |
| RBC 018 | 22 | 26 | 18-5 | 4 | 52.48 | 84.5 | 0.58 | 35.4 | 0.29 | | 88 |
| RBC 018 | 26 | 30 | 18-6 | 4 | 45.91 | 80.5 | 0.66 | 31.5 | 0.28 | | 70 |
| RBC 018 | 30 | 35 | 18-7 | 5 | 43.03 | 80.0 | 0.84 | 32.4 | 0.29 | | 75 |
| RBC 020 | 3 | 6 | 20-1 | 3 | 47.33 | 69.0 | 1.43 | 34.5 | 1.04 | 2 | 92 |
| RBC 020 | 6 | 9 | 20-2 | 3 | 34.35 | 56.5 | 1.96 | 30.9 | 2.16 | | 87 |
| RBC 021 | 14 | 15 | 21-2 | 1 | 36.25 | 83.0 | 0.56 | 29.6 | 1.83 | | 76 |
| RBC 021 | 15 | 21 | 21-3 | 6 | 28.25 | 82.0 | 1.02 | 32 | 3.47 | <1 | 83 |
| RBC 025 | 8 | 11 | 25-1 | 3 | 53.70 | 82.0 | 0.57 | 37 | 0.49 | 5 | 91 |
| RBC 025 | 11 | 15 | 25-2 | 4 | 50.25 | 84.5 | 0.48 | 36.1 | 0.51 | 6 | 85 |
| RBC 025 | 15 | 18 | 25-3 | 3 | 49.03 | 84.0 | 0.31 | 34.1 | 0.56 | 7 | 72 |
| RBC 025 | 18 | 20 | 25-4 | 2 | 44.37 | 80.0 | 0.82 | 33.2 | 0.69 | 7 | 69 |
| RBC 025 | 20 | 23 | 25-5 | 3 | 43.91 | 79.0 | 0.9 | 33.1 | 0.61 | 6 | 71 |
| RBC 025 | 23 | 25 | 25-6 | 2 | 41.64 | 81.5 | 0.63 | 33 | 0.66 | 3 | 77 |
| RBC 028 | 5 | 7 | 28-1 | 2 | 35.09 | 81.5 | 0.96 | 31.3 | 0.5 | | 96 |
| RBC 028 | 7 | 12 | 28-2 | 5 | 46.70 | 81.5 | 0.94 | 35.4 | 0.39 | | 97 |
| RBC 028 | 12 | 14 | 28-3 | 2 | 48.26 | 76.0 | 0.99 | 35.2 | 0.42 | | 97 |
| RBC 028 | 14 | 18 | 28-4 | 4 | 45.39 | 81.5 | 0.94 | 34.6 | 0.39 | | 90 |
| RBC 028 | 18 | 21 | 28-5 | 3 | 36.81 | 76.0 | 1.6 | 34.6 | 0.64 | 12 | 77 |
| RBC 034 | 4 | 6 | 34-1 | 2 | 39.67 | 77.5 | 0.55 | 35.2 | 0.42 | 9 | 83 |
| RBC 034 | 6 | 8 | 34-2 | 2 | 45.17 | 74.5 | 0.65 | 32.8 | 0.42 | 2 | 79 |
| RBC 034 | 8 | 11 | 34-3 | 3 | 43.54 | 81.5 | 0.46 | 32.1 | 0.48 | | 73 |
| RBC 034 | 11 | 13 | 34-4 | 2 | 39.35 | 85.0 | 0.84 | 31.1 | 0.59 | 5 | 65 |
| RBC 034 | 13 | 15 | 34-5 | 2 | 38.06 | 73.5 | 1.87 | 26.2 | 0.46 | | 62 |
| RBC 035 | 4 | 10 | 35-1 | 6 | 50.74 | 82.0 | 0.49 | 34.8 | 0.39 | 1 | 84 |
| RBC 035 | 10 | 11 | 35-2 | 1 | 46.58 | 87.0 | 0.65 | 33.5 | 0.37 | 5 | 73 |
| RBC 035 | 11 | 12 | 35-3 | 1 | 45.80 | 81.0 | 1.1 | 35.6 | 1.01 | 2 | 78 |
| RBC 035 | 12 | 14 | 35-4 | 2 | 43.19 | 85.0 | 1.02 | 31.8 | 0.39 | 8 | 63 |
| RBC 035 | 14 | 16 | 35-5 | 2 | 31.35 | 63.5 | 2.38 | 28.5 | 0.45 | 3 | 55 |
| RBC 037 | 5 | 8 | 37-1 | 3 | 47.78 | 66.5 | 1.59 | 36.3 | 0.45 | 6 | 89 |
| RBC 037 | 9 | 12 | 37-2 | 3 | 55.86 | 75.0 | 2.12 | 36.6 | 0.39 | | 94 |
| RBC 037 | 13 | 17 | 37-3 | 4 | 56.46 | 65.5 | 2.61 | 33.2 | 0.62 | | 79 |
| RBC 037 | 20 | 22 | 37-4 | 2 | 45.28 | 56.0 | 2.77 | 29.6 | 0.55 | | 58 |
| RBC 038 | 5 | 8 | 38-1 | 3 | 50.56 | 80.5 | 0.92 | 36.4 | 0.76 | 12 | 82 |

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| RBC 038 | 8 | 10 | 38-2 | 2 | 51.59 | 82.0 | 0.8 | 37.5 | 0.56 | 19 | 77 |
| RBC 038 | 10 | 13 | 38-3 | 3 | 50.59 | 82.5 | 0.76 | 37.3 | 0.49 | 12 | 84 |
| RBC 038 | 15 | 17 | 38-4 | 2 | 54.69 | 79.0 | 1.29 | 36.3 | 0.37 | 16 | 75 |
| RBC 038 | 17 | 21 | 38-5 | 4 | 48.20 | 74.0 | 1.28 | 33.4 | 0.41 | 5 | 69 |
| RBC 038 | 21 | 23 | 38-6 | 2 | 42.04 | 75.0 | 1 | 34 | 0.45 | 3 | 75 |
| RBC 039 | 9 | 11 | 39-1 | 2 | 48.37 | 79.5 | 0.68 | 36.8 | 0.51 | <1 | 96 |
| RBC 039 | 11 | 13 | 39-2 | 2 | 49.32 | 76.5 | 0.87 | 35.2 | 0.51 | | 88 |
| RBC 039 | 14 | 16 | 39-3 | 2 | 45.58 | 78.0 | 0.99 | 34.5 | 0.51 | 1 | 83 |
| RBC 039 | 16 | 19 | 39-4 | 3 | 32.67 | 74.0 | 1.25 | 29.7 | 0.46 | 3 | 76 |
| RBC 045 | 5 | 9 | 45-1 | 4 | 49.11 | 86.5 | 0.22 | 37.5 | 0.44 | | 97 |
| RBC 045 | 9 | 13 | 45-2 | 4 | 50.76 | 86.5 | 0.28 | 37.6 | 0.3 | 13 | 82 |
| RBC 045 | 13 | 15 | 45-3 | 2 | 53.38 | 85.0 | 0.27 | 34.2 | 0.36 | 6 | 75 |
| RBC 045 | 15 | 18 | 45-4 | 3 | 38.82 | 80.0 | 0.81 | 31.3 | 0.42 | 13 | 58 |
| RBC 046 | 6 | 7 | 46-1 | 1 | 17.28 | 57.0 | 1.45 | 26.7 | 0.45 | 6 | 75 |
| RBC 046 | 7 | 9 | 46-2 | 2 | 22.04 | 59.5 | 1.19 | 29.7 | 0.42 | 14 | 74 |
| RBC 047 | 7 | 9 | 47-1 | 2 | 53.92 | 78.0 | 0.41 | 37.9 | 0.31 | 10 | 86 |
| RBC 047 | 9 | 12 | 47-2 | 3 | 55.73 | 84.5 | 0.34 | 37.5 | 0.35 | 20 | 77 |
| RBC 047 | 12 | 18 | 47-3 | 6 | 58.66 | 86.5 | 0.21 | 37.9 | 0.34 | 16 | 81 |
| RBC 047 | 18 | 22 | 47-4 | 4 | 61.08 | 87.0 | 0.2 | 36.1 | 0.25 | 7 | 84 |
| RBC 048 | 5 | 6 | 48-1 | 1 | 48.57 | 76.5 | 0.61 | 36.2 | 0.64 | 28 | 67 |
| RBC 048 | 6 | 7 | 48-2 | 1 | 65.33 | 72.5 | 0.6 | 37 | 0.47 | 8 | 89 |
| RBC 048 | 7 | 12 | 48-3 | 5 | 64.74 | 80.0 | 0.36 | 37.9 | 0.45 | 4 | 92 |
| RBC 048 | 12 | 16 | 48-4 | 4 | 55.20 | 85.5 | 0.49 | 36.4 | 0.46 | 9 | 83 |
| RBC 048 | 16 | 19 | 48-5 | 3 | 39.42 | 77.5 | 1.04 | 32.2 | 0.46 | 12 | 63 |
| RBC 049 | 4 | 6 | 49-1 | 2 | 34.07 | 75.0 | 1.47 | 29.4 | 0.56 | 1 | 73 |
| RBC 049 | 6 | 12 | 49-2 | 6 | 18.79 | 58.5 | 0.82 | 25.4 | 1.08 | 7 | 68 |
| RBC 050 | 4 | 6 | 50-1 | 2 | 50.96 | 72.0 | 1.55 | 34.9 | 0.43 | | 93 |
| RBC 050 | 6 | 8 | 50-2 | 2 | 71.19 | 76.5 | 1.56 | 36.9 | 0.26 | | 97 |
| RBC 050 | 8 | 13 | 50-3 | 5 | 54.08 | 78.5 | 1.3 | 32.7 | 0.31 | | 86 |
| RBC 057 | 6 | 7 | 57-1 | 1 | 22.49 | 51.5 | 2.16 | 29.3 | 0.69 | 7 | 77 |
| RBC 057 | 7 | 10 | 57-2 | 3 | 51.13 | 80.5 | 0.55 | 36.8 | 0.55 | 8 | 87 |
| RBC 057 | 10 | 14 | 57-3 | 4 | 56.41 | 81.5 | 0.47 | 37.5 | 0.55 | 8 | 87 |
| RBC 057 | 14 | 15 | 57-4 | 1 | 55.91 | 81.5 | 0.51 | 37.3 | 0.6 | 8 | 89 |
| RBC 057 | 15 | 17 | 57-5 | 2 | 53.24 | 81.5 | 0.56 | 37.4 | 0.33 | | 95 |
| RBC 057 | 17 | 20 | 57-6 | 3 | 52.57 | 81.5 | 0.62 | 37.2 | 0.5 | 1 | 94 |
| RBC 057 | 20 | 23 | 57-7 | 3 | 53.25 | 80.0 | 0.6 | 37.3 | 0.47 | 7 | 88 |
| RBC 058 | 5 | 9 | 58-1 | 4 | 37.44 | 80.0 | 0.74 | 33.6 | 0.46 | | 94 |
| RBC 058 | 9 | 12 | 58-2 | 3 | 43.95 | 84.5 | 0.69 | 33.8 | 0.4 | | 97 |
| RBC 058 | 12 | 15 | 58-3 | 3 | 55.90 | 80.5 | 0.92 | 34.2 | 0.36 | | 83 |
| RBC 058 | 15 | 20 | 58-4 | 5 | 43.12 | 82.0 | 0.66 | 32.2 | 0.47 | | 78 |
| RBC 060 | 4 | 5 | 60-1 | 1 | 40.09 | 74.0 | 1 | 34.2 | 0.33 | 2 | 86 |
| RBC 060 | 5 | 8 | 60-2 | 3 | 35.12 | 82.0 | 0.47 | 34.1 | 0.43 | <1 | 90 |
| RBC 060 | 8 | 10 | 60-3 | 2 | 47.80 | 83.5 | 0.48 | 34.8 | 0.47 | | 89 |
| RBC 060 | 10 | 13 | 60-4 | 3 | 54.79 | 84.0 | 0.49 | 34.2 | 0.37 | | 79 |
| RBC 060 | 13 | 15 | 60-5 | 2 | 47.83 | 81.0 | 0.71 | 34.1 | 0.59 | | 77 |
| RBC 060 | 15 | 20 | 60-6 | 5 | 40.48 | 80.0 | 0.76 | 33.5 | 0.55 | | 77 |
| RBC 060 | 20 | 22 | 60-7 | 2 | 41.20 | 76.5 | 1.02 | 31 | 0.56 | <1 | 63 |
| RBC 060 | 22 | 26 | 60-8 | 4 | 44.55 | 74.0 | 1.23 | 29.1 | 0.78 | 4 | 49 |
| RBC 061 | 4 | 6 | 61-2 | 2 | 53.60 | 81.0 | 0.91 | 35.2 | 0.29 | | 87 |
| RBC 061 | 6 | 9 | 61-3 | 3 | 59.36 | 75.0 | 0.93 | 34 | 0.67 | | 85 |
| RBC 061 | 9 | 11 | 61-4 | 2 | 50.08 | 78.0 | 0.94 | 34.3 | 0.43 | | 84 |
| RBC 061 | 11 | 13 | 61-5 | 2 | 53.91 | 80.5 | 0.73 | 37.1 | 0.45 | | 87 |
| RBC 061 | 13 | 16 | 61-6 | 3 | 55.07 | 74.0 | 0.89 | 33.1 | 0.33 | | 74 |
| RBC 061 | 16 | 19 | 61-7 | 3 | 43.75 | 73.5 | 0.95 | 29.2 | 0.4 | | 53 |
| RBC 061 | 19 | 23 | 61-8 | 4 | 36.89 | 77.0 | 0.85 | 31.9 | 0.49 | 2 | 61 |

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| RBC 061 | 23 | 25 | 61-9 | 2 | 37.69 | 66.5 | 1.4 | 31.2 | 0.5 | | 58 |
| RBC 061 | 25 | 28 | 61-10 | 3 | 36.42 | 76.0 | 0.76 | 29 | 0.42 | | 50 |
| RBC 061 | 28 | 29 | 61-11 | 3 | 31.44 | 66.0 | 1.6 | 26.3 | 0.44 | 2 | 29 |

# JORC Code, 2012 Edition – Table 1 report-Burracoppin

## Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

| Criteria | JORC Code explanation | Commentary |
|---|---|---|
| *Sampling techniques* | • *Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.*<br>• *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.*<br>• *Aspects of the determination of mineralisation that are Material to the Public Report.*<br>• *In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.* | • Samples were taken at 1m intervals downhole using an industry standard air-core rig with an open blade bit.<br>• Samples were returned via compressed air via the drill string inner tube.<br>• The entire metre for each sample was collected into green plastic sample bags and placed sequentially on the surface next to the drill hole.<br>• Each sample was logged and a matchbox sized sub-sample was retained in chip trays.<br>• Sample composites were then designed based on logging and collected using a spearing technique diagonally through the main sample from top to bottom with a piece of PVC pipe.<br>• Approximately 1 – 2kg of sample material was collected to make up each composite sample. |
| *Drilling techniques* | • *Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).* | • Air-core drilling using an open blade bit. |
| *Drill sample recovery* | • *Method of recording and assessing core and chip sample recoveries and results assessed.*<br>• *Measures taken to maximise sample recovery and ensure representative nature of the samples.*<br>• *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to* | • Entire 1m samples collected into green plastic bags and laid sequentially next to the drillhole. |

| Criteria | JORC Code explanation | Commentary |
|---|---|---|
| | *preferential loss/gain of fine/coarse material.* | |
| *Logging* | • *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.*<br>• *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.*<br>• *The total length and percentage of the relevant intersections logged.* | • Samples logged in the field primarily for lithology and colour onto hard copy log sheets, then transferred into excel spreadsheets in the office.<br>• Representative sub-samples collected into chip trays. |
| *Sub-sampling techniques and sample preparation* | • *If core, whether cut or sawn and whether quarter, half or all core taken.*<br>• *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.*<br>• *For all sample types, the nature, quality and appropriateness of the sample preparation technique.*<br>• *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.*<br>• *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.*<br>• *Whether sample sizes are appropriate to the grain size of the material being sampled.* | • Sample composites were designed based on logging information and collected in the field.<br>• A spearing technique was used to collect sub samples from each plastic sample bag into fine weave calico bags according to composite design.<br>• Spearing was performed diagonally through the main sample from top to bottom with a piece of PVC pipe.<br>• Approximately 1-2kg of sample material was collected to make up each composite sample. No sub sampling conducted in the field.<br>• Equivalent sized sub-samples were collected from each metre sample.<br>• Sample preparation was conducted by Bureau Veritas in the laboratory according to industry standard techniques.<br>• Sample preparation involved:<br>- Dry, weigh and stage crush to -6.3mm<br>- Liberation using blunging followed by wet screen to +180um, -180 to +45um, -45um.<br>- Filter, dry and weigh each size fraction. |
| *Quality of assay data and laboratory tests* | • *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.*<br>• *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.*<br>• *Nature of quality control procedures adopted (eg standards, blanks,* | • Laboratory techniques are industry standard.<br>• The -45ųm sample was sub sampled into splits for analysis of brightness, XRF, ICP analysis and XRD analysis to determine chemical compositions and mineralogical compositions respectively.<br>• XRF used to determine elemental contents.<br>• ICP with fusion digest used to determine rare earth element contents.<br>• XRD used to determine Halloysite and Kaolinite content. |

| Criteria | JORC Code explanation | Commentary |
|---|---|---|
| | *duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.* | |
| *Verification of sampling and assaying* | • *The verification of significant intersections by either independent or alternative company personnel.*<br>• *The use of twinned holes.*<br>• *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.*<br>• *Discuss any adjustment to assay data.* | • Verification was conducted with the use of blanks and repeats in the laboratory.<br>• No field duplicates taken. |
| *Location of data points* | • *Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.*<br>• *Specification of the grid system used.*<br>• *Quality and adequacy of topographic control.* | • Sample points recorded in the field with handheld GPS. Sample locations align with aerial photography of sample sites.<br>• Topographic information extracted from Copernicus GLO 30 Digital Elevation Model for the Burracoppin project area. The data packet was contoured in QGIS and exported to Micromine as contour strings. The contour strings were restricted within an external boundary string and a DTM was created of the topographical surface. The Copernicus DEM has a 30m pixel resolution and a reported relative vertical accuracy of <2m for slopes below or equal to 20%. |
| *Data spacing and distribution* | • *Data spacing for reporting of Exploration Results.*<br>• *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.*<br>• *Whether sample compositing has been applied.* | • Drillholes located on a 400m grid in a diamond pattern.<br>• Samples taken at 1m intervals downhole.<br>• Samples composited for submission to the lab based on geological logging.<br>• Samples composited predominantly based on colour. |
| *Orientation of data in relation to geological structure* | • *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.*<br>• *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.* | • Holes drilled vertically into an undulating but flat lying weathering profile above the underlying granite. |
| *Sample security* | • *The measures taken to ensure sample security.* | • Samples delivered directly to the lab by geologist. |
| *Audits or reviews* | • *The results of any audits or reviews of sampling techniques and data.* | • No audits or reviews conducted. |

## Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

| Criteria | JORC Code explanation | Commentary |
|---|---|---|
| *Mineral tenement and land tenure status* | • *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.*<br>• *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.* | • E70/5708 and E77/2774 were acquired by Ragusa Minerals Limited as announced 5 July 2021.<br>• Both tenements are in good standing. |
| *Exploration done by other parties* | • *Acknowledgment and appraisal of exploration by other parties.* | • No other exploration conducted previously. |
| *Geology* | • *Deposit type, geological setting and style of mineralisation.* | • Weathered kaolinite outcropping in places but mostly covered with superficial recent soils. Kaolinised profile extends down to a maximum of approximately 60m before transitioning to fresh granite. |
| *Drill hole Information* | • *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:*<br>o *easting and northing of the drill hole collar*<br>o *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar*<br>o *dip and azimuth of the hole*<br>o *down hole length and interception depth*<br>o *hole length.*<br>• *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.* | • All drilling information including collar and assay data included in the body of the report. |
| *Data aggregation methods* | • *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.*<br>• *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should* | • No data aggregation.<br>• No top caps or bottom caps applied to the data set. |

| Criteria | JORC Code explanation | Commentary |
|---|---|---|
| | *be shown in detail.*<br>• *The assumptions used for any reporting of metal equivalent values should be clearly stated.* | |
| *Relationship between mineralisation widths and intercept lengths* | • *These relationships are particularly important in the reporting of Exploration Results.*<br>• *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.*<br>• *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').* | • Downhole intersections represent true thickness of the mineralised body in that location. |
| *Diagrams* | • *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.* | • Plan and sections of sample locations attached. |
| *Balanced reporting* | • *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.* | • All samples reported |
| *Other substantive exploration data* | • *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.* | • Not applicable |
| *Further work* | • *The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).*<br>• *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.* | • Initial testwork to be conducted on a sub set of samples with elevated REE to test for amenity for liberation.<br>• Closer spaced drilling will be conducted to improve and expand on the current mineral resource estimation. |

**Section 3 Estimation and Reporting of Mineral Resources**

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

| Criteria | JORC Code explanation | Commentary |
|---|---|---|
| *Database integrity* | • *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between* | • All data was loaded directly from laboratory ascii files into excel and checked for duplicated data, missing data, sample intervals, etc. |

| Criteria | JORC Code explanation | Commentary |
|---|---|---|
| | *its initial collection and its use for Mineral Resource estimation purposes.*<br>• *Data validation procedures used.* | • Data validated visually in excel and spatially in 3D space within Micromine. |
| *Site visits* | • *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.*<br>• *If no site visits have been undertaken indicate why this is the case.* | • The Cp has visited site many times, supervised some of the drilling and carried out some of the logging and sampling. |
| *Geological interpretation* | • *Confidence in (or conversely, the uncertainty of ) the geological interpretation of the mineral deposit.*<br>• *Nature of the data used and of any assumptions made.*<br>• *The effect, if any, of alternative interpretations on Mineral Resource estimation.*<br>• *The use of geology in guiding and controlling Mineral Resource estimation.*<br>• *The factors affecting continuity both of grade and geology.* | • High confidence is placed in the geological interpretation given the relatively simple nature of the deposit with reference to the data spacing. Confidence in the distribution of REE and halloysite in particular is reduced do to the variable nature of these components.<br>• No alternative interpretation possible. No folding or significant faulting evident within the project area. Any alternative model of erosional or weathering surfaces is considered to only have a mild impact on the outcome.<br>• Geology is used to guide the estimation only in relation to weathering surfaces. |
| *Dimensions* | • *The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.* | • The mineral resource estimation covers an area of approximately 2.65km in the east – west direction and 3.16km in the north – south direction. The resource varies vertically significantly due to interactions between weathering and erosional surfaces and ranges from 0m (basement outcrop) to 52m. Depth to mineralisation ranges from <1m (immediately below topsoil) to approximately 13m at its deepest. |
| *Estimation and modelling techniques* | • *The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.*<br>• *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.*<br>• *The assumptions made regarding recovery of by-products.*<br>• *Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).*<br>• *In the case of block model interpolation, the block size in relation to the average* | • Micromine mining software was used for data preparation, geological modelling and data interpolation into a prototype model of the area.<br>• The model was constructed using parent cell sizes of X = 100, Y = 100, Z = 1 with sub cells down to X = 10, Y = 10 and Z = 0.5 at zone interfaces.<br>Cell were centred on drill holes and there were 3 floating parent cells between fixed data points in both the X and the Y directions. Cells in the Z direction were designed with 1 sample per cell.<br>• Statistics and variograpy were performed on a number of key variables to establish appropriate search parameters.<br>• Trial ordinary kriging against inverse distance interpolation runs were conducted to determine a preferred interpolation method. OK was deemed to excessively smooth the spatially limited data set so ID was the preferred method.<br>• Interpolation was conducted in separate |

| Criteria | JORC Code explanation | Commentary |
|---|---|---|
| | *sample spacing and the search employed.*<br>• *Any assumptions behind modelling of selective mining units.*<br>• *Any assumptions about correlation between variables.*<br>• *Description of how the geological interpretation was used to control the resource estimates.*<br>• *Discussion of basis for using or not using grade cutting or capping.*<br>• *The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.* | stages for different variables subject to their individual characteristics. The interpolated model was successively built at each stage.<br>• Interpolation for each variable was conducted in rounds of successively larger searches with decreasing confidence with the search round recorded within the cell.<br>• Estimation parameters have been listed in the body of the announcement.<br>• Validation was conducted visually against drill hole data and the interpolation parameters were adjusted to suit on a iterative basis if results were not acceptable at any given point during the estimation. |
| *Moisture* | • *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.* | • Tonnages are estimated on an in-situ dry basis using an assumed universal density of 1.53 g/cm3.<br>• No moisture data has been incorporated |
| *Cut-off parameters* | • *The basis of the adopted cut-off grade(s) or quality parameters applied.* | • The global cut-off grade of ISO-B 70 was applied based on assumed blended saleable quality.<br>• The 400ppm TREO cut-off was adopted from several similar third party values used. The commercial basis for this is yet to be determined. |
| *Mining factors or assumptions* | • *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.* | • Based mining assumptions for shallow strip mining in free digging material were used.<br>• The CP is of the opinion the deposit meets the criteria for reasonable prospects for eventual economic extraction based on similar currently operating kaolinite mines |
| *Metallurgical factors or assumptions* | • *The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.* | • No metallurgical factors have been taken into account. |

| Criteria | JORC Code explanation | Commentary |
|---|---|---|
| *Environmen-tal factors or assumptions* | • *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.* | • No assumptions have been made regarding residue disposal.<br>• It is anticipated the clay and REE components will be extracted and sold leaving a majority fine quartz sand residue of approximately 50% of the volume mined.<br>• This may also be sold as an industrial product or backfilled into the void after mining.<br>• An operation is expected to chemical additive free and produce an inert tail. |
| *Bulk density* | • *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.*<br>• *The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.*<br>• *Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.* | • A uniform bulk density of 1.53 g/cm3 was applied to the estimated mineralized zones as in-situ dry bulk density. This figure was derived from the neighbouring project which lies directly adjacent to the Burracoppin project on its eastern side. The neighbouring project assumed the value of 1.53 g/cm3 based on similar kaolinized granite deposits in Australia, with values ranging from 1.4 g/cm3 - 1.9 g/cm3. |
| *Classification* | • *The basis for the classification of the Mineral Resources into varying confidence categories.*<br>• *Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).*<br>• *Whether the result appropriately reflects the Competent Person's view of the deposit.* | • The entire resource is categorised as inferred in accordance with the JORC code (2012).<br>• Data density is not sufficient for any higher categorisation at this stage. |
| *Audits or reviews* | • *The results of any audits or reviews of Mineral Resource estimates.* | • No audits or reviews have been conducted. |
| *Discussion of relative accuracy/ confidence* | • *Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits,* | • The accuracy of the mineral resource estimate is reflected in the inferred category assigned to the estimate and is considered the appropriate level of confidence for this data set.<br>• The estimate is considered global based on the relatively sparse data set and is considered to have an inferred level of confidence at a global scale. Locally, the |

| Criteria | JORC Code explanation | Commentary |
|---|---|---|
| | *or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.*<br>• *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.*<br>• *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.* | estimates may have greater variability although this attempted to be accounted for with the estimation methodology employed.<br>• The deposit is not mined so comparison against production data is not possible. |